A co-planar four-link mechanism with four revolute joints (R-R-R-R) is known as a four bar mechanism. Like the slider-crank mechanism and its kinematic inversions (R-R-R-P) it is one of the basic building blocks of many machines.

After covering kinematic and force analysis in general we will concentrate on four-bar mechanisms.

All uses of a four-bar can be categorized in one of these three groups:

- 1. Correlation of Crank Angles / Function Generation
- $\theta_{14} = f(\theta_{12})$



By Ackermann.svg: User:Bromsklossderivative work: Andy Dingley (talk) - Ackermann.svg, CC BY-SA 3.0, https://commons.wikimedia.org/w/index.php?curid=11038290

All uses of a four-bar can be categorized in one of these three groups:

1. Correlation of Crank Angles / Function Generation

 $\theta_{14} = f(\theta_{12})$ $y = x^2$



https://www.youtube.com/watch?v=HAdjYblt3hM

- All uses of a four-bar can be categorized in one of these three groups:
- 1. Correlation of Crank Angles / Function Generation
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https://www.youtube.com/watch?v=noL5D4jLW6A

- All uses of a four-bar can be categorized in one of these three groups:
- 2. Coupler point curve



https://www.youtube.com/watch?v=4U8aREBFIDE

- All uses of a four-bar can be categorized in one of these three groups:
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https://www.youtube.com/watch?v=NZZtXUcRZVs

- All uses of a four-bar can be categorized in one of these three groups:
- 2. Coupler point curve



https://www.youtube.com/watch?v=ESpEFJZp-co

- All uses of a four-bar can be categorized in one of these three groups:
- 3. Positions of Coupler Link / Rigid Body Guidance



https://www.youtube.com/watch?v=TLROAYXxkvA

Grashof's Rule:

- The motion characteristics of a four-bar mechanism will depend on the ratio of link lengths.
- The links that are connected to the fixed link may have one of these two types of motion:
- The link may have a full rotation around the fixed axis. This is called a *crank* (crank is also used for the input link)
- The link may oscillate between two limiting angles. This is called a *rocker*.

Grashof's Rule:

A four-bar mechanism may have one of the following three types of motion:

- Both links connected to the fixed link can have full rotation. This is called *double crank* or *drag link* mechanism.
- Both links connected to the fixed link can oscillate between two limiting positions. This is called *double rocker* mechanism.
- One of the links connected to the fixed link oscillates between two limiting positions while other can make full rotation. This is called *crank rocker* mechanism.

Grashof's Rule:

- ℓ : Length of the longest link
- s: Length of the shortest link
- p, q: lengths of the two intermediate links
- 1. If $\ell + s$
 - a. Two different crank-rocker mechanisms are possible. In either case shortest link is the crank and the fixed link is either of the adjacent links.
 - b. One drag link (double crank) is possible when the shortest link is fixed.
 - c. One double rocker mechanism is possible when the link opposite to the shortest is fixed.

Grashof's Rule:

2. If $\ell + s > p + q$

Only four different double rocker mechanisms are possible.

3. If $\ell + s = p + q$

Same as case 1 however these mechanisms suffer from a condition known as *change point position*. At this position all the link center lines are collinear and this is a kinematically singular (undetermined) position. The follower at this position may rotate in either direction. The sign (σ) that determines the closure is subject to change at this position.

Dead-Center Positions of a *Crank Rocker* Mechanism: *Grashof's Rule*

 $\ell + s ,$ *s*is the crank

a. Two different crank-rocker mechanisms are possible. In either case shortest link is the crank and the fixed link is either of the adjacent links.

2. Kinematic Analysis

Velocity and Acceleration Analyses

Four-Bar Mechanism

$$a_{2}e^{i\theta_{12}} + a_{3}e^{i\theta_{13}} = a_{1} + a_{4}e^{i\theta_{14}}$$
Re: $a_{2}cos\theta_{12} + a_{3}cos\theta_{13} = a_{1} + a_{4}cos\theta_{14}$ (1)
Im: $a_{2}sin\theta_{12} + a_{3}sin\theta_{13} = a_{4}sin\theta_{14}$ (2)
(1): $-\dot{\theta}_{12}a_{2}sin\theta_{12} - \dot{\theta}_{13}a_{3}sin\theta_{13} = -\dot{\theta}_{14}a_{4}sin\theta_{14}$
(2): $\dot{\theta}_{12}a_{2}cos\theta_{12} + \dot{\theta}_{13}a_{3}cos\theta_{13} = \dot{\theta}_{14}a_{4}cos\theta_{14}$
Let θ_{12} , $\dot{\theta}_{12}$ and $\ddot{\theta}_{12}$ be the input:
$$\begin{bmatrix} -a_{3}sin\theta_{13} & a_{4}sin\theta_{14} \\ a_{3}cos\theta_{13} & -a_{4}cos\theta_{14} \end{bmatrix} \begin{bmatrix} \dot{\theta}_{13} \\ \dot{\theta}_{14} \end{bmatrix} = \begin{bmatrix} a_{2}sin\theta_{12} \\ -a_{2}cos\theta_{12} \end{bmatrix} \dot{\theta}_{12}$$
 $\dot{\theta}_{14} = \frac{a_{2}sin(\theta_{12} - \theta_{13})}{a_{4}sin(\theta_{14} - \theta_{13})} \dot{\theta}_{12} = g_{24}\dot{\theta}_{12}$

 $\dot{\theta}_{14} = 0$ when $sin(\theta_{12} - \theta_{13}) = 0 \rightarrow \begin{cases} \theta_{12} - \theta_{13} = 0, \text{ Extended dead center} \\ \theta_{12} - \theta_{13} = \pi, \text{ Folded dead center} \end{cases}$





Dead-Center Positions of a Crank Rocker Mechanism:

 $\theta_{12} - \theta_{13} = 0$, Extended dead center





 $\theta_{12} - \theta_{13} = \pi$, Folded dead center

Transmission Angle:

Alt^[1] defined the transmission angle as:

 $tan\mu = \frac{F_3^a}{F_2^p} \text{ or } sin\mu = \frac{F_3^a}{F_2}$

[1] Alt, Hermann (1889 - 1954). Der Übertragungswinkel und seine Bedeutung für das Konstruieren periodischer Getriebe (The transmission angle and its importance for designing periodic mechanisms). Werkstattstechnik 26 (1932) 61-64. $F_3 \angle \theta_{13} + \pi$





5. Four Bar Mechanism



$$cos\mu = \frac{a_3^2 + a_4^2 - a_1^2 - a_2^2 + 2a_1a_2cos\theta_{12}}{2a_3a_4}$$

The extremums of the transmission angle is

$$\frac{d\mu}{d\theta_{12}} = \sin\theta_{12} = 0 \rightarrow \begin{cases} \theta_{12} = 0\\ \theta_{12} = \pi \end{cases}$$

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Transmission Angle:



Mechanical Advantage:

<u>Definition</u>: The mechanical advantage of a mechanism is the instantaneous ratio of output torque (force) to input torque (force).

For a four bar mechanism where input is link 2 and output is link 4 $$F_{3^{\angle\theta_{13}+\pi}}$$



Mechanical Advantage:

$$MA = \frac{T_{14}}{T_{12}}$$

Neglecting friction, kinetic and gravitational potential energy changes of the links

$$\mathbb{P}_{in} = \mathbb{P}_{out}$$
$$-T_{12}\omega_{12} = T_{14}\omega_{14}$$
$$MA = \frac{T_{14}}{T_{12}} = -\frac{\omega_{12}}{\omega_{14}}$$

Mechanical Advantage:

 $MA = \frac{T_{14}}{T_{12}} = -\frac{\omega_{12}}{\omega_{14}} = -\frac{\dot{\theta}_{12}}{\dot{\theta}_{14}} = \frac{a_4 \sin(\theta_{14} - \theta_{13})}{a_2 \sin(\theta_{12} - \theta_{13})}$

 $sin(\theta_{12} - \theta_{13}) = 0, MA \rightarrow \infty$ Dead centers! $sin(\theta_{14} - \theta_{13}) = 0, MA = 0, \mu = 0$





Body Guidance-Two Position Synthesis:

<u>Chasles Theorem</u>: The motion of a rigid body from one position to another in plane motion occurs most simply by a rotation about the pole P_{12} which is located at the perpendicular bisectors of two pairs of *homologous points*.

Please note that when the separation between the two positions of the plane diminishes the homologous points define the velocity and the pole P_{12} boils down to instant center of zero velocity (ICZV).

Body Guidance-Two Position Synthesis:

Chasles Theorem:

