EE-464 STATIC POWER CONVERSION-II

Resonant Converters

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- Reduces transformer size



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Disadvantages of High Switching Frequency?

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Disadvantages of High Switching Frequency?

Increased switching losses

Switching Loss



You have more turn-on, turn-off energy dissipation as the frequency increases

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Two main types of switching:

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• when voltage is zero (ZVS)

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- when voltage is zero (ZVS)
- when current is zero (ZCS)

There are many resonant converter topologies.

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- . Resonant Switch Converters
- Load Resonant Converter
- . Resonant DC-link Converter





Minimum impedance at resonant frequency



- Series RLC Circuit Animation
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- Signal Transmission and Reflection

Resonant Switch Converter: Zero Current Switching

W. Hart., Power Electronics, Ch.9

Resonant Switch Converter: Zero Current Switching

W. Hart., Power Electronics, Ch.9



Assumption: L_o is large enough, I_o is constant

Operating Mode: t < 0

Operating Mode: t < 0



Switch open, Diode ON (frewheeling), $v_C=0$

Operating Mode: $0 < t < t_1$

Operating Mode: $0 < t < t_1$



Switch closed, L_r start charging

 $i_L < I_o$ so the diode is still ON



When $i_L = I_o$, the diode turns OFF

Excess inductor current charges the capacitor $v_C>0$

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If no action is taken, oscillation starts in the LC circuit!
Turn the switch off, when $i_L=0$

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=Zero current switching!

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Alternatively a unidirectional switch (SCR) can be used.



Very small switching loss (due to capacitances in the switch)

Output current is supplied by C (discharges linearly)

Initial Mode: $t_3 \, < t < T$

Initial Mode: $t_3 \, < t < T$



 $v_C=0$, diode starts freewheeling,

Switch ready to to turn ON (zero current)

W. Hart., Power Electronics, Ch.9-2



Operating Mode: $0 < t < t_1$

Inductor Lr sees constant Vs voltage and the current increases linearly

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$$t_1 = rac{I_o L_r}{V_s}$$

Diode is off, capacitor voltage starts building up:

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$$v_c(t) = V_s - L_r rac{di_L(t)}{dt}$$

Differentiating and solving second order LC circuit (as in Ch9.2)

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$$i_L(t)=I_o+rac{V_s}{Z_o}sin\omega_0(t-t_1)$$



$$\omega_0=rac{1}{\sqrt{L_rC_r}}$$

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Differentiating and solving second order LC circuit (as in Ch9.2)

$$i_L(t)=I_o+rac{V_s}{Z_o}sin\omega_0(t-t_1)$$
 .

 $Z_0=\sqrt{rac{L_r}{C_r}}$

$$\omega_0=rac{1}{\sqrt{L_rC_r}}$$

$$t_2 - t_1 = rac{1}{\omega_0} [sin^{-1} (rac{-I_0 Z_0}{V_s})]$$

Capacitor voltage can be expressed as:

$$V_c(t)=V_s[1-cos(\omega_0(t-t_1))]$$

which implies capacitor voltage can reach up to 2 Vs (a disadvantage of resonant converters)

As the inductor current reaches to zero at t2, the switch can be openced with no current (ZCS)

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Capacitor discharges with constant load current.

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$$V_c(t)=rac{I_0}{C_r}(t_2-t)+V_c(t_2)$$

If Vc=0 at t3:

$$t_3 - t_2 = rac{C_r v_c(t_2)}{I_o} = rac{C_r V_s [1 - cos(\omega_o(t_2 - t_1))]}{I_o}$$

In this interval switch is off (diode freewheeling)

The length of this invertal directly controls the output voltage.

The switching frequency should be adjusted so that t3 is less than period (T).

Use energy balance (L-C are lossless)

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$$V_o = V_s f_s [rac{t_1}{2} + (t_2 - t_1) + (t_3 - t_2)]$$

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$$V_o = V_s f_s [rac{t_1}{2} + (t_2 - t_1) + (t_3 - t_2)]$$

 $V_o \, < \, V_s\,$ operates as a buck converter

Output voltage is controlled by the switching frequency!

Time internals are a function of output current

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Load changes switching frequency must be changed



Example (Hart 9-1)

Resonant Switch Converter: Zero Voltage Switching

W. Hart., Power Electronics, Ch.9

Resonant Switch Converter: Zero Voltage Switching

W. Hart., Power Electronics, Ch.9



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Operating Mode: t < 0

Operating Mode: t < 0



D1 off, switch ON,
$$i_L = I_o$$

Operating Mode: $0 < t < t_1$

Operating Mode: $0 < t < t_1$



Switch opened, v_C start charging linearly


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Operating Mode: $t_1 \, < t < t_2$

Operating Mode: $t_1 \, < t < t_2$



When $v_C = V_s$, the diode (D1) is forward biased

LC resonant circuit start oscillating,

When $v_C = 0$, the diode (Ds) turns on to carry iL. (which is negative) $^{33/70}$



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Operating Mode: $t_2 \, < t < t_3$

Operating Mode: $t_2\, < t < t_3$



Ds is ON, $V_L = V_s$, inductor current increases linearly

Switch should be closed just after Ds turns on (zero voltage switching)

When $i_{T} = I_{-}$ D1 is off and back to the initial position

Initial Mode: $t_3 \, < t < T$

Initial Mode: $t_3 \, < t < T$



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Output voltage=?

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Output voltage = Average of v_x(t)
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$$v_x(t) = V_s(1-t/t_1)$$
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 $v_x(t) = 0$ for $t_1 < t < t_3$

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$$arphi_x(t)$$

 $v_x(t) = V_s(1-t/t_1)$ for $0 < t < t_1$
 $v_x(t) = 0$ for $t_1 < t < t_3$
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 $v_x(t) = V_s$ for $t_3 < t < T$

Calculate the average voltage

Output voltage

Output voltage

$$V_o=rac{V_s}{T}[rac{t_1}{2}+(T-t_3)]$$

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or

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Output voltage

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or

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Output voltage is controlled by varying fs

 $V_o \, < \, V_s$, buck converter



Output voltage is controlled by varying fs



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Phasor equivalent circuit



Frequency Response

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Add a diode rectifier to the output of the series resonant inverter

Add a diode rectifier to the output of the series resonant inverter



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Variations of the Resonant Converters

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LLC Resonant Converter

Variations of the Resonant Converters

LLC Resonant Converter



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Resonant Converter (Wireless Power Transfer)



<u>Qi Wireless Charging</u>

<u>Multi-Coil Wireless Charger</u>

Resonant Converter (Wireless Power Transfer)



BMW Electric Car Charger

Resonant Converter (Wireless Power Transfer)



Linearization and Control of Series-Series WPT

Various Configurations

For curious students: Overview of resonant circuits



Dunning-Kruger Effect

Dunning-Kruger Effect


<u>Dunning-Kruger Effect</u>



Dunning-Kruger Effect



Education in EEE

<u>ODTÜ Elektrik size neler kattı?</u>

Drawing

You can download this presentation from: <u>keysan.me/ee464</u>

Extras

Alternative ZCS Converter

Mohan Section 9.5



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Add a diode rectifier to the output of the series resonant inverter

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Simplified Equivalent Circuit

Simplified Equivalent Circuit



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Continuous Conduction Mode with $\omega_s > \omega_0$



Figure 9-13 SLR dc-dc converter; continuous-conduction mode with $\omega_s > \omega_0$.

Continuous Conduction Mode with $\omega_s > \omega_0$

- iL is approximately sinusoidal
- Switches turn on at zero voltage (no turn-on losses)
- but they turn-off at non-zero current (turn-off losses exist)

Continuous Conduction Mode with $\omega_0/2 < \omega_s < \omega_0$



Figure 9-12 SLR dc-dc converter; continuous-conduction mode with $\frac{1}{2}\omega_0 < \omega_s < \omega_0$. 64 / 70

Continuous Conduction Mode with $\omega_0/2 < \omega_s < \omega_0$

- T+ conducts less than 180 degrees
- Switches turn on with finite voltage (turn-on losses exist)
- Switches turn-off with zero current (no turn-off losses)
- Turn-off occurs naturally, so thyristors can be used

Discontinuous Conduction Mode with $\omega_s < \omega_0/2$



Figure 9-11 SLR dc-dc converter; discontinuous-conduction mode with $\omega_s < \frac{1}{2}\omega_0$.

Discontinuous Conduction Mode with $\omega_s < \omega_0/2$

- iL is zero for some time (discontinuous conduction)
- Switches turn on at zero current, with finite voltage
- Switches turn-off naturally with zero current (no turn-off losses)
- Thyristors can be used
- Disadvantage: Relatively large peak current in the circuit

Parallel Resonant Converter

Parallel Resonant Converter



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Resonant DC Link Converter

Resonant DC Link Converter



3-Phase Resonant DC Link Converter

3-Phase Resonant DC Link Converter

