

SOLUTIONS

Problem 1. (Shigley)

6-14 Given: AISI 1006 CD steel, $F = 0.55$ N, $P = 8.0$ kN, and $T = 30$ N · m, applying the DE theory to stress elements A and B with $S_y = 280$ MPa

$$\begin{aligned} \text{A:} \quad \sigma_x &= \frac{32Fl}{\pi d^3} + \frac{4P}{\pi d^2} = \frac{32(0.55)(10^3)(0.1)}{\pi(0.020^3)} + \frac{4(8)(10^3)}{\pi(0.020^2)} \\ &= 95.49(10^6) \text{ Pa} = 95.49 \text{ MPa} \end{aligned}$$

$$\tau_{xy} = \frac{16T}{\pi d^3} = \frac{16(30)}{\pi(0.020^3)} = 19.10(10^6) \text{ Pa} = 19.10 \text{ MPa}$$

$$\sigma' = (\sigma_x^2 + 3\tau_{xy}^2)^{1/2} = [95.49^2 + 3(19.1)^2]^{1/2} = 101.1 \text{ MPa}$$

$$n = \frac{S_y}{\sigma'} = \frac{280}{101.1} = 2.77 \quad \text{Ans.}$$

$$\text{B:} \quad \sigma_x = \frac{4P}{\pi d^3} = \frac{4(8)(10^3)}{\pi(0.020^2)} = 25.47(10^6) \text{ Pa} = 25.47 \text{ MPa}$$

$$\begin{aligned} \tau_{xy} &= \frac{16T}{\pi d^3} + \frac{4V}{3A} = \frac{16(30)}{\pi(0.020^3)} + \frac{4}{3} \left[\frac{0.55(10^3)}{(\pi/4)(0.020^2)} \right] \\ &= 21.43(10^6) \text{ Pa} = 21.43 \text{ MPa} \end{aligned}$$

$$\sigma' = [25.47^2 + 3(21.43^2)]^{1/2} = 45.02 \text{ MPa}$$

$$n = \frac{280}{45.02} = 6.22 \quad \text{Ans.}$$

Problem 2. (Shigley)

6-39 (a) Ignoring stress concentration

$$F = S_y A = 160(4)(0.5) = 320 \text{ kips} \quad \text{Ans.}$$

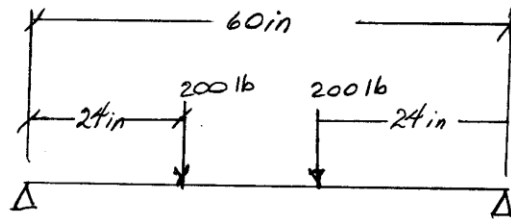
(b) From Fig. 6-36: $h/b = 1$, $a/b = 0.625/4 = 0.1563$, $\beta = 1.3$

$$\text{Eq. (6-51)} \quad 70 = 1.3 \frac{F}{4(0.5)} \sqrt{\pi(0.625)}$$

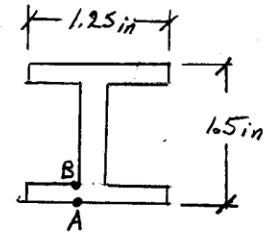
$$F = 76.9 \text{ kips} \quad \text{Ans.}$$

Problem 3.

Given:



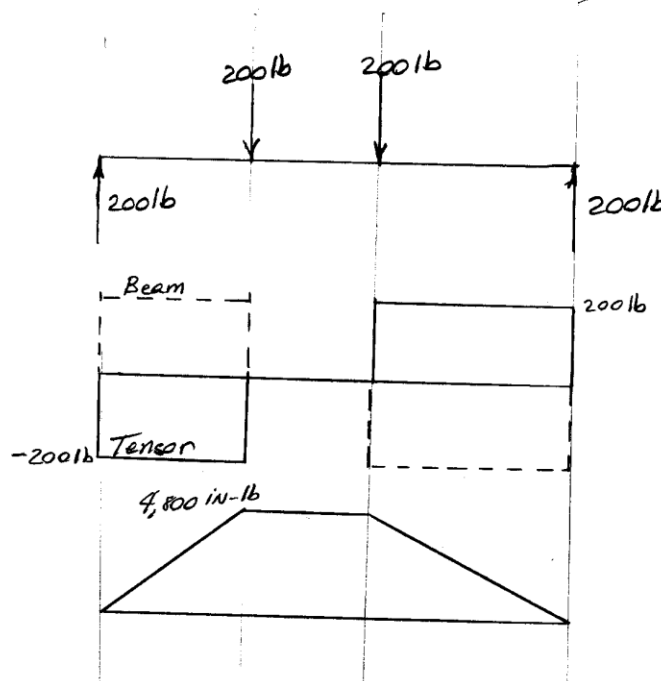
$$S_y = 50 \text{ ksi}$$



Web and flange thickness = 0.125 in

- Find: (a) Bending and transverse shear stress at A & B.
 (b) Maximum normal and maximum shear stress.
 (c) Factor of safety based on maximum normal and maximum shear stress.

Solution: Find maximum shear force and bending moment.



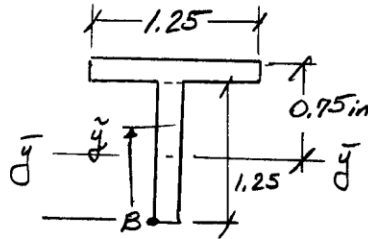
Note that tensor sign convention is used.

$$V_{\max} = \pm 200 \text{ lb}$$

$$M_{\max} = 4,800 \text{ in-lb}$$

Compute cross section properties

Find φ_B



$$A = (1.25 \text{ in})(0.125 \text{ in}) + (1.25 \text{ in})(0.125 \text{ in}) = 0.3125 \text{ in}^2$$

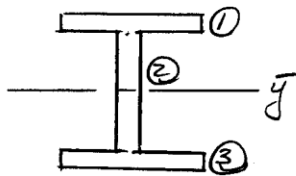
$$\tilde{y} = \frac{(1.25 \text{ in})(0.125 \text{ in})(1.25 + \frac{0.125}{2}) + (1.25)(0.125)(\frac{1.25}{2})}{0.3125}$$

$$= \frac{0.502}{0.3125} = 0.969 \text{ in}$$

$$\tilde{y} - \bar{y} = 0.969 \text{ in} - 0.625 = 0.344 \text{ in}$$

$$\varphi_B = A(\tilde{y} - \bar{y}) = \underline{\underline{0.1075 \text{ in}^3}}$$

Find I



$$I = \sum \bar{I} + (\tilde{y} - \bar{y})^2 A$$

$$= 2 \left(\frac{1}{12} (1.25 \text{ in})(0.125 \text{ in})^3 + (1.25 \text{ in})(0.125) \left(0.75 - \frac{0.125}{2} \right)^2 \right) + \frac{1}{12} (0.125 \text{ in})(1.25 \text{ in})^3$$

$$= \underline{\underline{0.168 \text{ in}^4}}$$

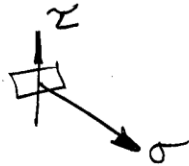
Part A

$$\begin{aligned} \text{Bending stress at A} \quad \sigma_A &= \frac{M C_A}{I} = \frac{(4,800 \text{ in-lb})(0.75 \text{ in})}{0.168 \text{ in}^4} \\ &= \underline{\underline{21.4 \text{ ksi}}} \end{aligned}$$

$$\begin{aligned} \text{Bending stress at B} \quad \sigma_B &= \frac{M C_B}{I} = \frac{(4,800 \text{ in-lb})(0.625 \text{ in})}{0.168 \text{ in}^4} \\ &= \underline{\underline{17.9 \text{ ksi}}} \end{aligned}$$

$$\text{Transverse shear stress at A} \quad \tau = \frac{V Q_A}{I t} = 0 \quad \text{since } Q_A = 0$$

$$\begin{aligned} \text{Transverse shear stress at B} \quad \tau &= \frac{V Q_B}{I t} = \frac{(200 \text{ lb})(0.1075 \text{ in}^3)}{(0.168 \text{ in}^4)(0.125 \text{ in})} \\ &= \underline{\underline{1.02 \text{ ksi}}} \end{aligned}$$



PART B

At point A the principal stresses are

$$\sigma_1 = \sigma = 21.4 \text{ ksi}, \quad \sigma_2 = \sigma_3 = 0 \quad \underline{\underline{\sigma_{\max} = 21.4 \text{ ksi}}}$$

At point B,

$$\sigma_1 = \frac{\sigma_x + \sigma_y}{2} + \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2} = 17.95 \approx 18.0 \text{ ksi}$$

$$\begin{aligned} \sigma_2 &= \frac{\sigma_x + \sigma_y}{2} - \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2} = -0.06 \text{ ksi} \\ \sigma_3 &= 0 \end{aligned} \quad \underline{\underline{\sigma_{\max} = 18.0 \text{ ksi}}}$$

Maximum shear stress at A $\tau_{max} = \frac{\sigma_1 - \sigma_3}{2} = \frac{21.4}{2} = \underline{\underline{10.7 \text{ ksi}}}$

at B $\tau_{max} = \frac{\sigma_1 - \sigma_3}{2} = \frac{18 - (-0.06)}{2}$
 $= 9.03 \text{ ksi}$

PART C

Maximum normal stress theory (Point A)

$$\frac{\tau_{max}}{S_y} = \frac{1}{N} \Rightarrow N = \frac{S_y}{\tau_{max}} = \frac{50 \text{ ksi}}{21.4 \text{ ksi}} = \underline{\underline{2.34}}$$

Maximum shear stress theory (Point A)

$$\frac{\sigma_1 - \sigma_3}{S_y} = \frac{1}{N} \Rightarrow N = \frac{S_y}{\sigma_1 - \sigma_3} = \frac{50 \text{ ksi}}{21.4 \text{ ksi}} = \underline{\underline{2.34}}$$

Maximum normal stress theory (Point B)

$$\frac{\tau_{max}}{S_y} = \frac{1}{N} \Rightarrow N = \frac{S_y}{\sigma_{max}} = \frac{50 \text{ ksi}}{18.0 \text{ ksi}} = \underline{\underline{2.78}}$$

Maximum shear stress theory (Point B)

$$N = \frac{S_y}{\sigma_1 - \sigma_2} = \frac{50 \text{ ksi}}{18.06} = \underline{\underline{2.77}}$$