

by
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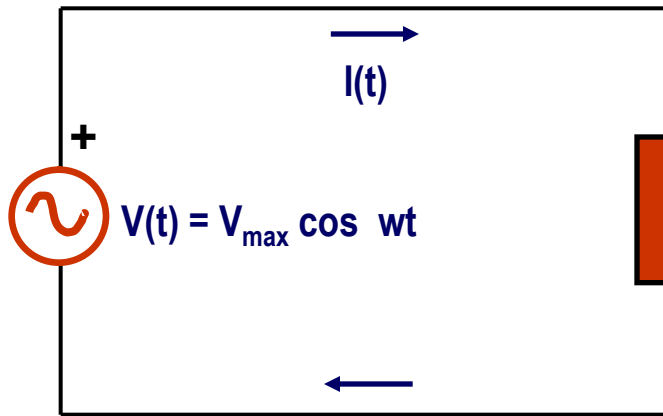
Voltage Waveform

Consider the following AC circuit driven by a source with voltage waveform;

$$V(t) = V_{max} \cos wt$$

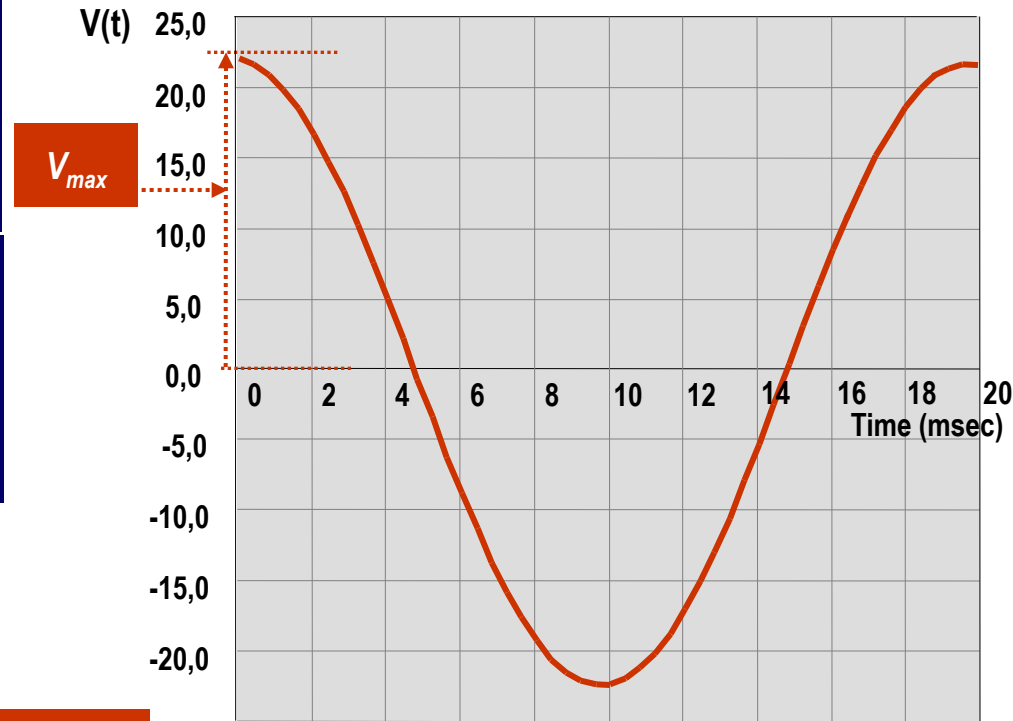
Phasor representation of this voltage waveform will then be

$$V_{max} \angle 0^\circ$$



$$\text{Load} = R + jX \\ = Z \angle \theta$$

$$Z = \sqrt{R^2 + X^2}, \theta = \tan^{-1}(X/R)$$



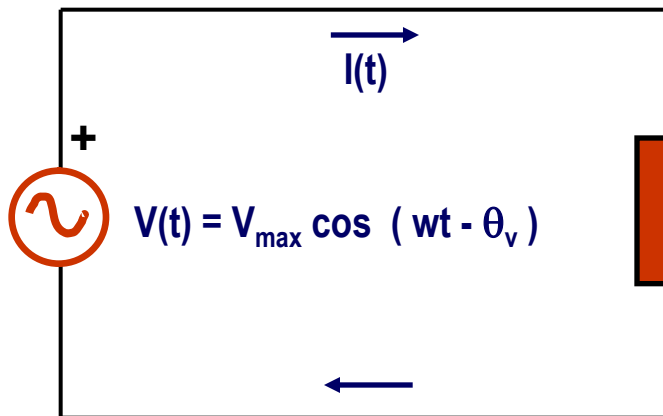
Phase Shift in Voltage Waveform

Consider now, the following AC circuit driven by a source with an AC voltage waveform;

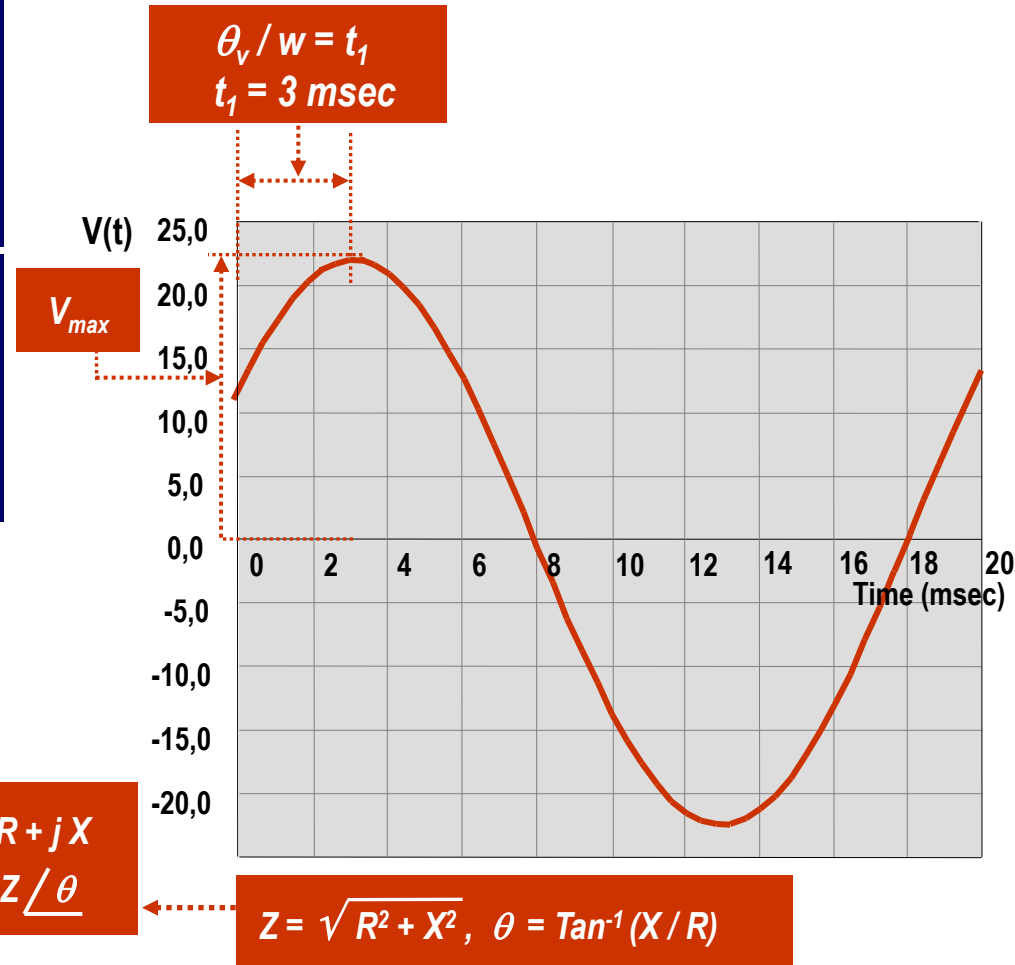
$$V(t) = V_{max} \cos (\omega t - \theta_v)$$

Phasor representation of the shifted voltage waveform will then be

$$V_{max} \angle -\theta_v$$



$$\text{Load} = R + jX \\ = Z \angle \theta$$



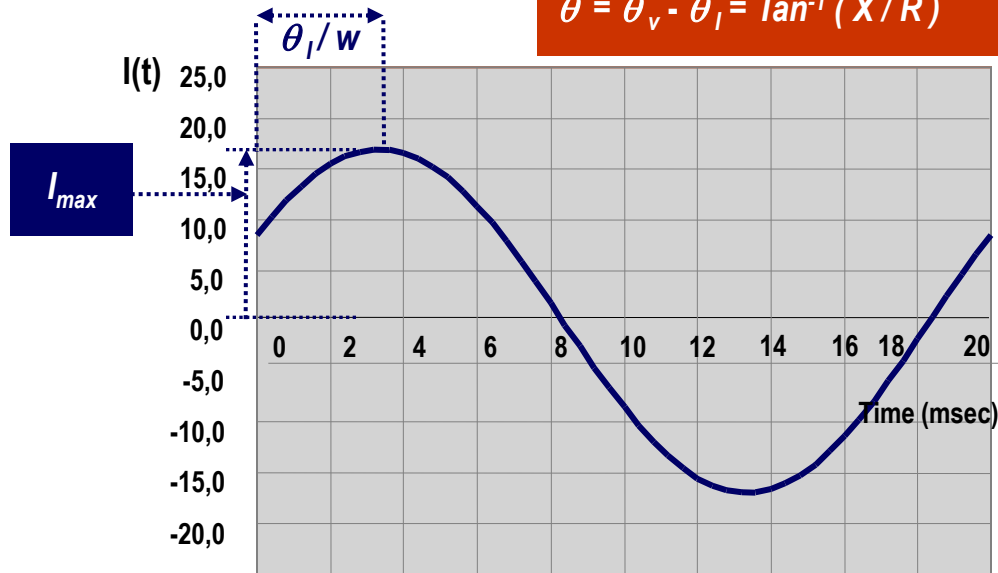
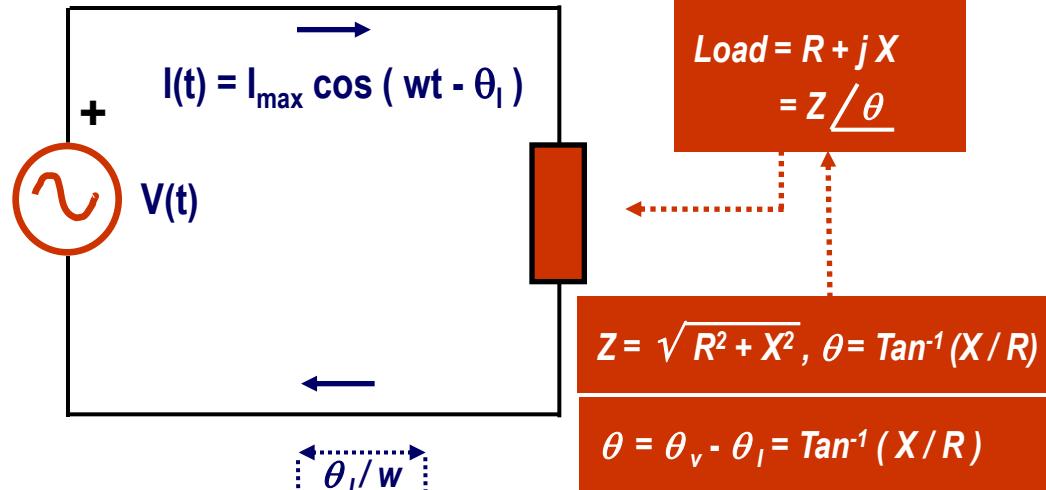
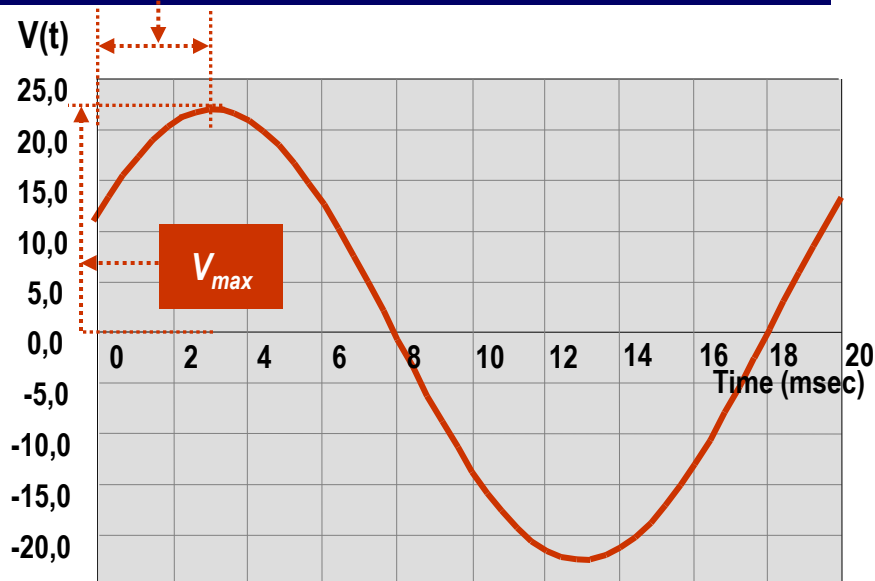
Current Waveform

Relation Between Voltage and Current Phasors

$$\frac{V_{max} \angle \theta_v}{Z \angle \theta} = I_{max} \angle -\theta_i$$

$$\theta_v / \omega = t_1$$

$$t_1 = 3 \text{ msec}$$



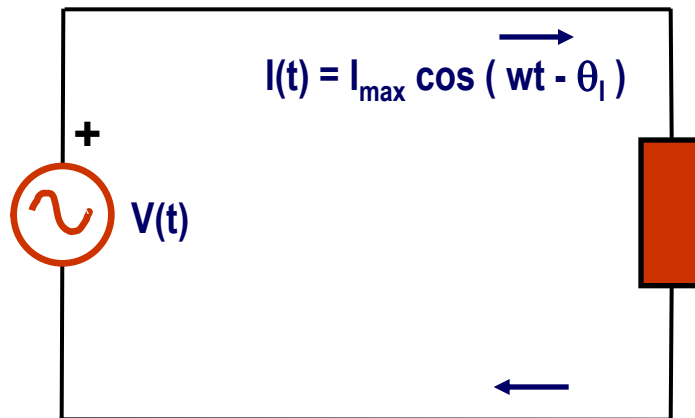
Current Waveform

Phasor representation of this current will then be

$$I_{max} \angle -\theta_I$$

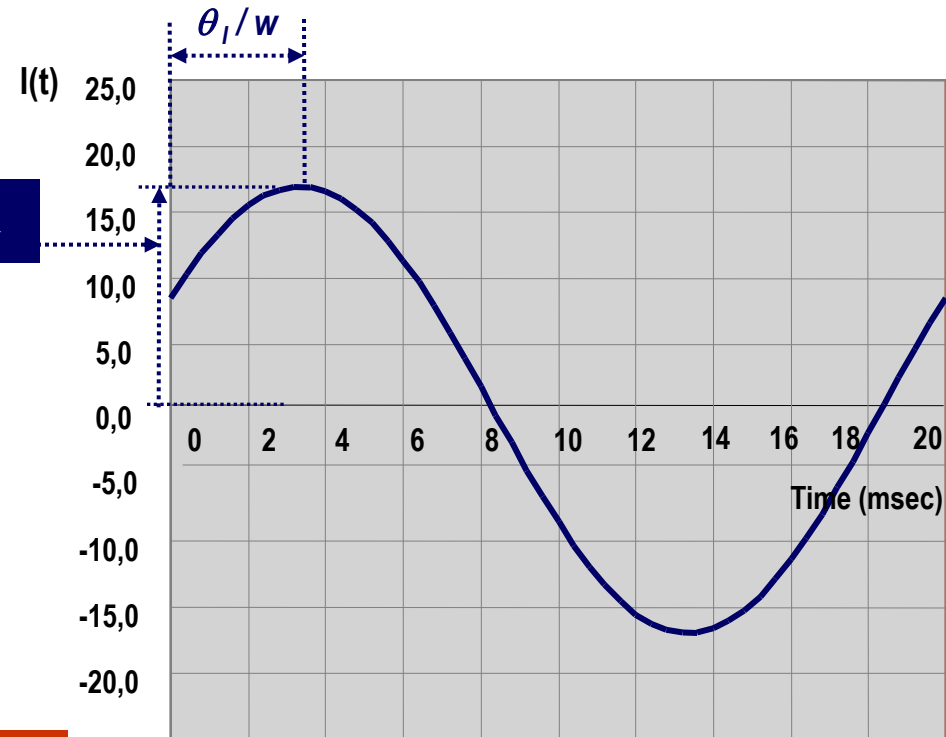
Waveform representation of this current will then be

$$I(t) = I_{max} \cos (\omega t - \theta_I)$$



$$\text{Load} = R + jX \\ = Z \angle \theta$$

$$Z = \sqrt{R^2 + X^2}, \quad \theta_I = \tan^{-1} (X / R)$$



Voltage and Current Waveforms

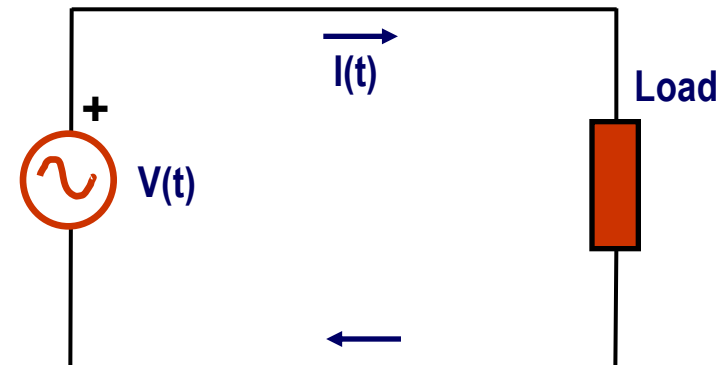
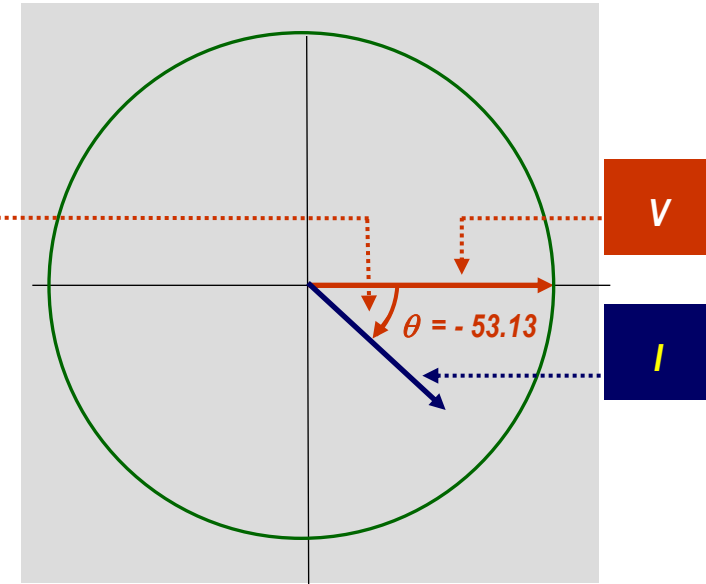
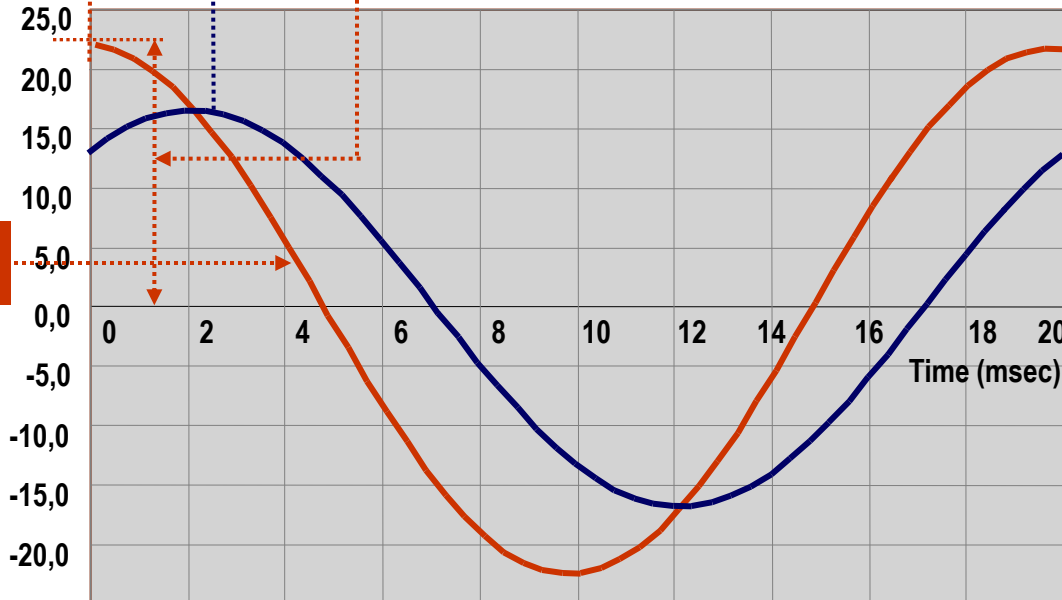
Please note that the angle difference $\theta_v - \theta_i$ depends only on the resistance R and reactance X of the load

$$\theta = \theta_v - \theta_i = \tan^{-1}(X/R)$$

$$\theta/w = (\theta_v - \theta_i)/w$$

V_{max}

$V(t)$



AC Power - Power Expression

Voltage and current waveforms are

$$V(t) = V_{max} \cos wt$$

$$I(t) = I_{max} \cos (wt - \theta)$$

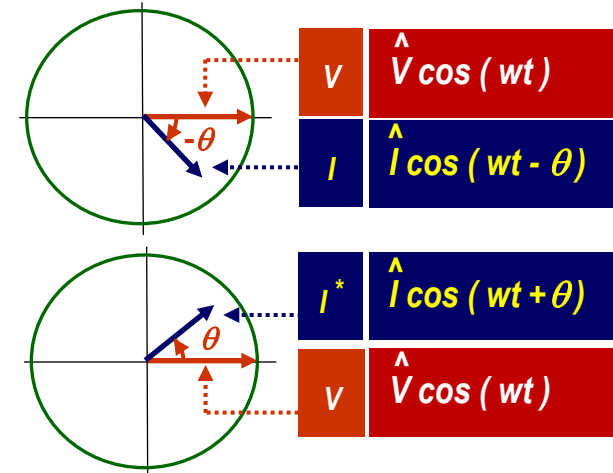
Power waveform will then be

$$S(t) = V(t) \times I(t)^*$$

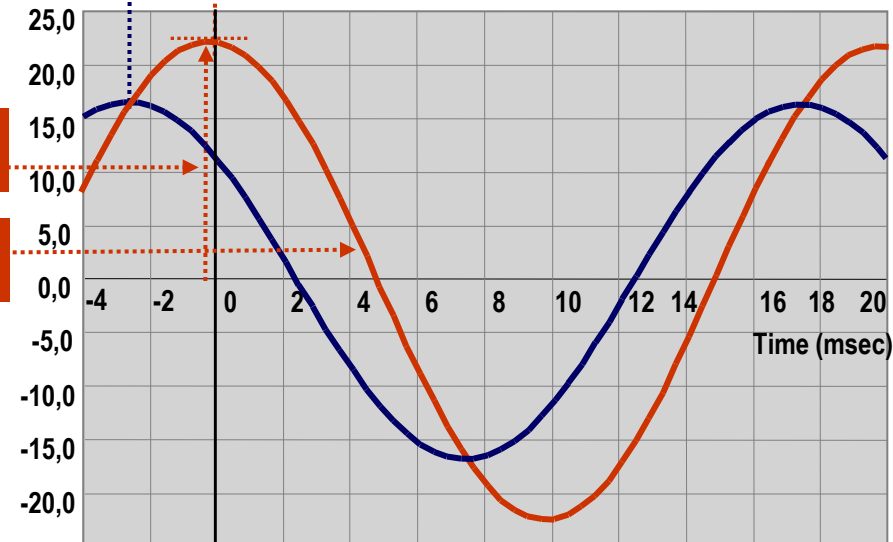
$$= V_{max} \cos wt \times I_{max} \cos (wt + \theta)$$

Please note that;
“-” sign here has
been altered due to
the conjugation
operation in the
definition of power:

$$S = V \times I^*$$



$$\theta / w = (\theta_v - \theta_i) / w$$



$$\cos (a + b) = \cos a \cos b - \sin a \sin b$$

$$\cos (a - b) = \cos a \cos b + \sin a \sin b$$

$$\cos (a + b) + \cos (a - b) = 2 \cos a \cos b$$

$$\cos a \cos b = \frac{1}{2} [\cos (a + b) + \cos (a - b)]$$

AC Power - Power Expression

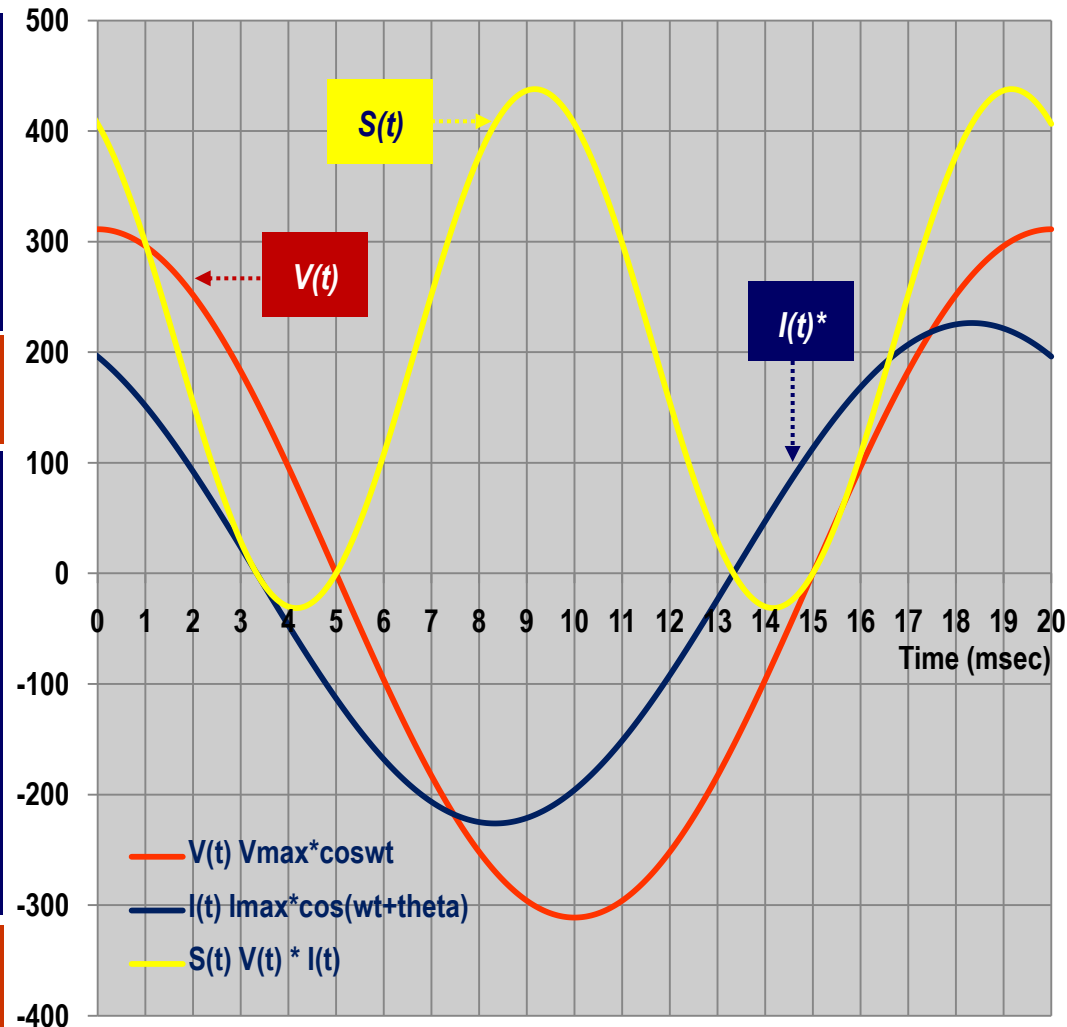
Power waveform is the product of the voltage and conjugate of the current waveforms

$$S(t) = V_{\max} I_{\max} \cos wt \times \cos (wt + \theta)$$

$$\cos a \times \cos b = \frac{1}{2} [\cos (a + b) + \cos (a - b)]$$

$$\begin{aligned} S(t) &= \frac{1}{2} V_{\max} I_{\max} [\cos (wt + wt + \theta) + \cos (wt - wt - \theta)] \\ &= \frac{1}{2} V_{\max} I_{\max} [\cos (2wt + \theta) + \cos \theta] \\ &= (V_{\max} / \sqrt{2}) (I_{\max} / \sqrt{2}) [\cos (2wt + \theta) + \cos \theta] \\ &= V_{\text{rms}} I_{\text{rms}} [\cos (2wt + \theta) + \cos \theta] \end{aligned}$$

$$V_{\text{rms}} = V_{\max} / \sqrt{2} \quad \theta = \theta_v - \theta_i = \tan^{-1}(X/R)$$



AC Power – Decomposition of Power Expression

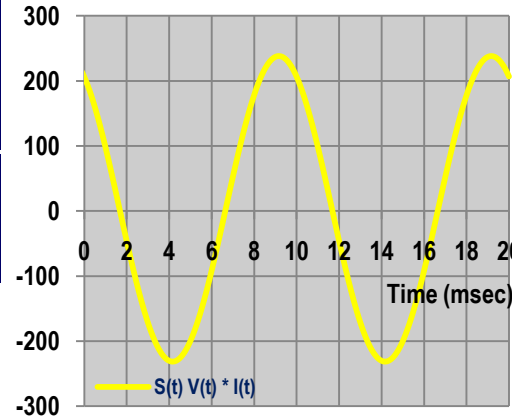
Power expression may be decomposed into two components

$$S(t) = V_{rms} I_{rms} \cos(2\omega t + \theta) + V_{rms} I_{rms} \cos \theta$$

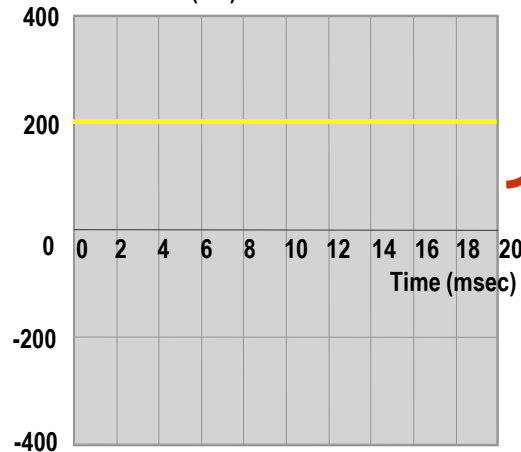
Sinusoidal (AC) Term

Constant (DC) Term

Sinusoidal (AC) Term

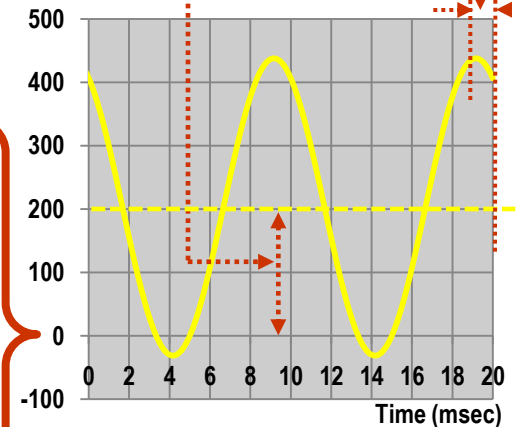


Constant (DC) Term



DC Term = $S(t)_{avg}$

θ / ω



AC Power – Average Power Expression

Average Power

$$S(t) = V_{rms} I_{rms} [\cos(2\omega t + \theta) + \cos \theta]$$

$$S(t)_{avg} = (1/T) \int_0^T S(t) dt$$

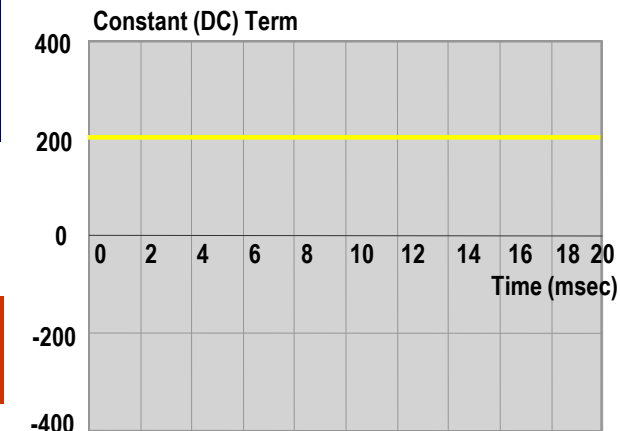
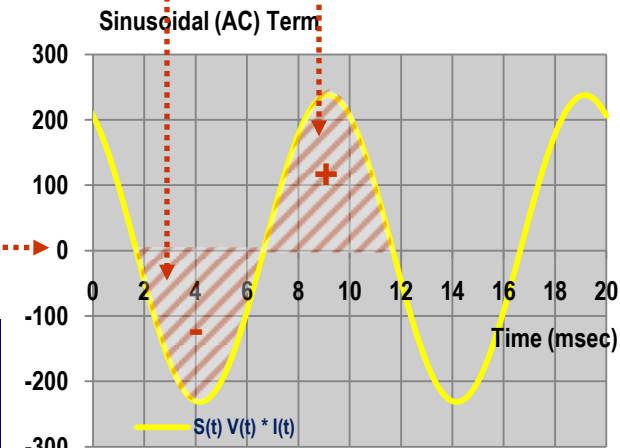
$$\begin{aligned} S(t)_{avg} &= (1/T) \int P(t) dt \\ &= (1/T) \int V_{rms} I_{rms} [\cos(2\omega t + \theta) + \cos \theta] dt \\ &= (1/T) \int V_{rms} I_{rms} \cos(2\omega t + \theta) dt + (1/T) \int V_{rms} I_{rms} \cos \theta dt \end{aligned}$$

zero

Constant (DC) Term

Average is zero

Sum of these areas is zero

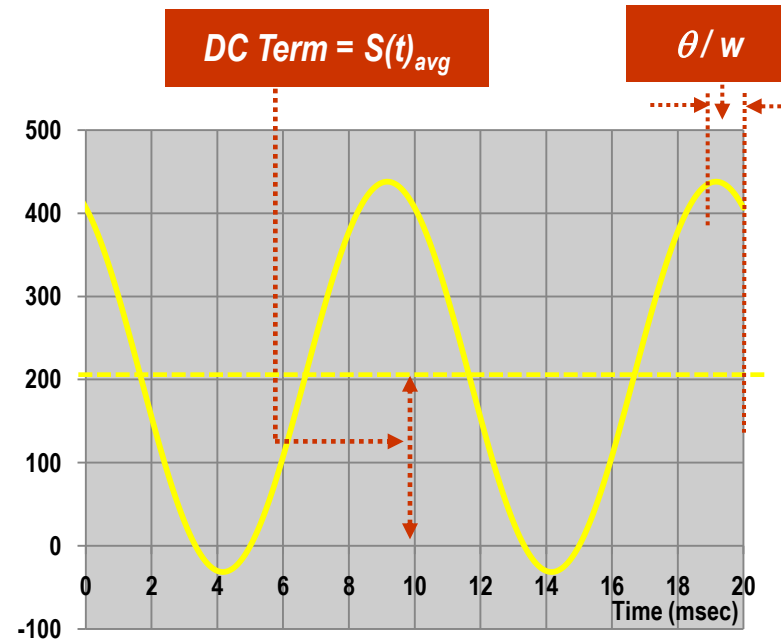
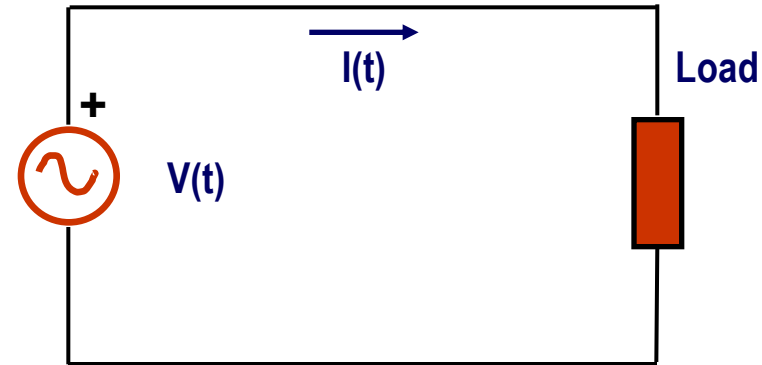


AC Power – Average Power Expression

Average Power

$$\begin{aligned}
 S(t)_{avg} &= (1/T) \int P(t) dt \\
 &= (1/T) V_{rms} I_{rms} \int \cos \theta dt \\
 &= (1/T) V_{rms} I_{rms} \cos \theta \left(\int dt \right) \leftarrow \int_0^T dt = T \\
 &= (1/T) T V_{rms} I_{rms} \cos \theta \\
 &= V_{rms} I_{rms} \cos \theta
 \end{aligned}$$

$$S(t)_{avg} = V_{rms} I_{rms} \cos \theta$$



Example

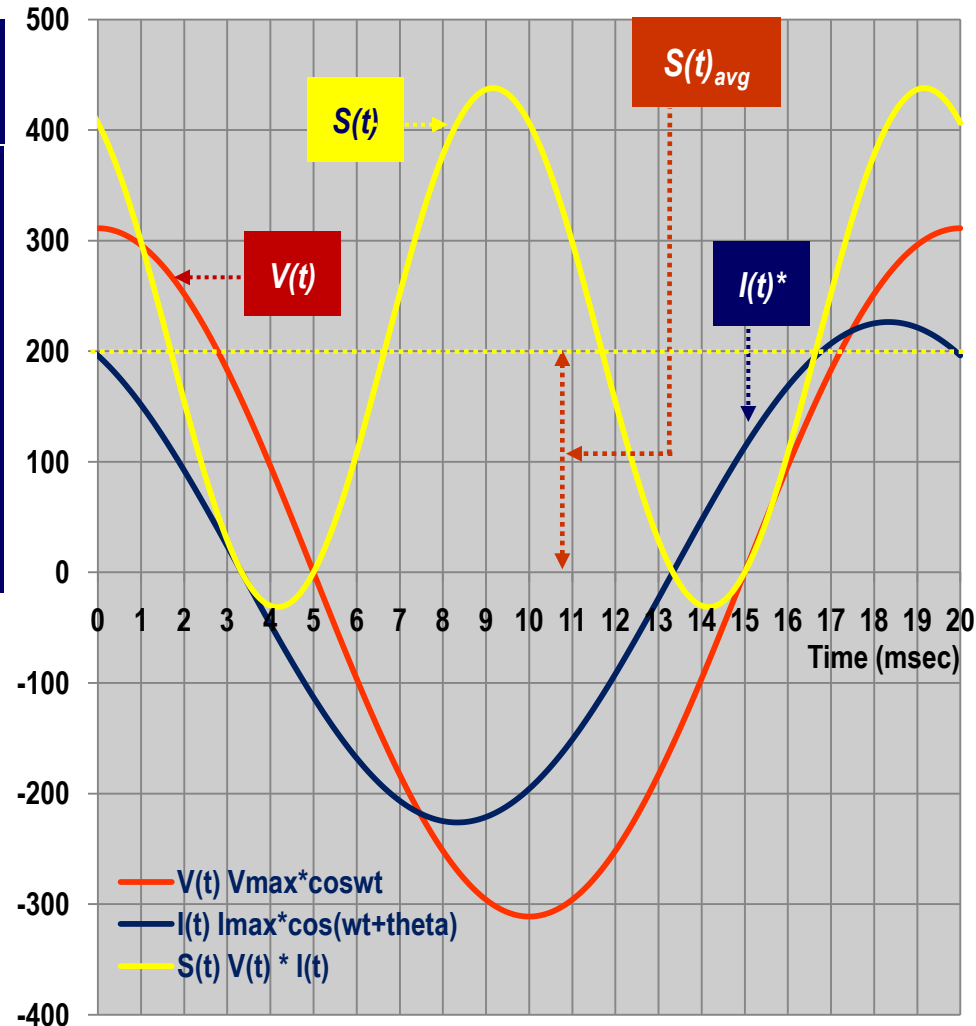
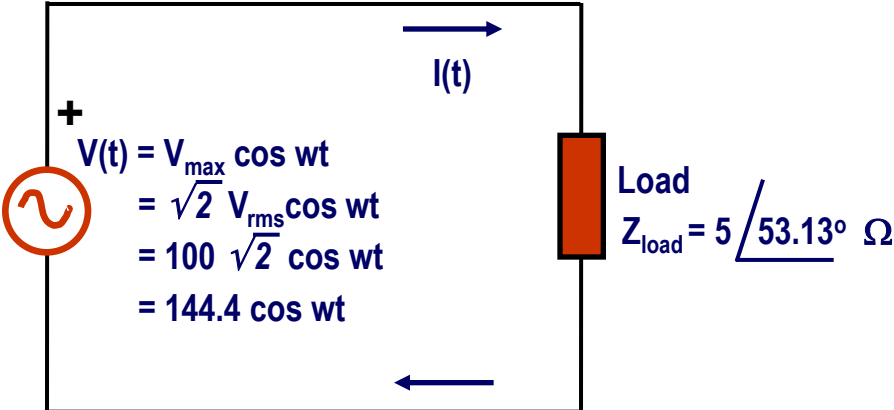
Question

Calculate the average and instantaneous powers dissipated in the load shown below

Parameters:

$$V_{rms} = 100 \text{ Volts}$$

$$Z_{load} = 3 + j4 \text{ Ohms} = 5 \angle 53.13^\circ \text{ Ohms}$$

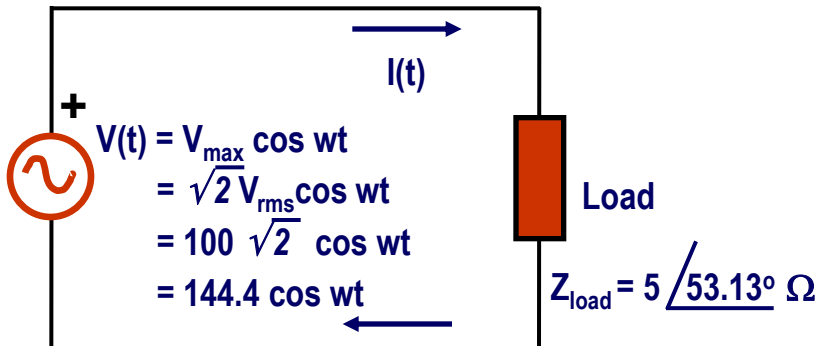


Solution

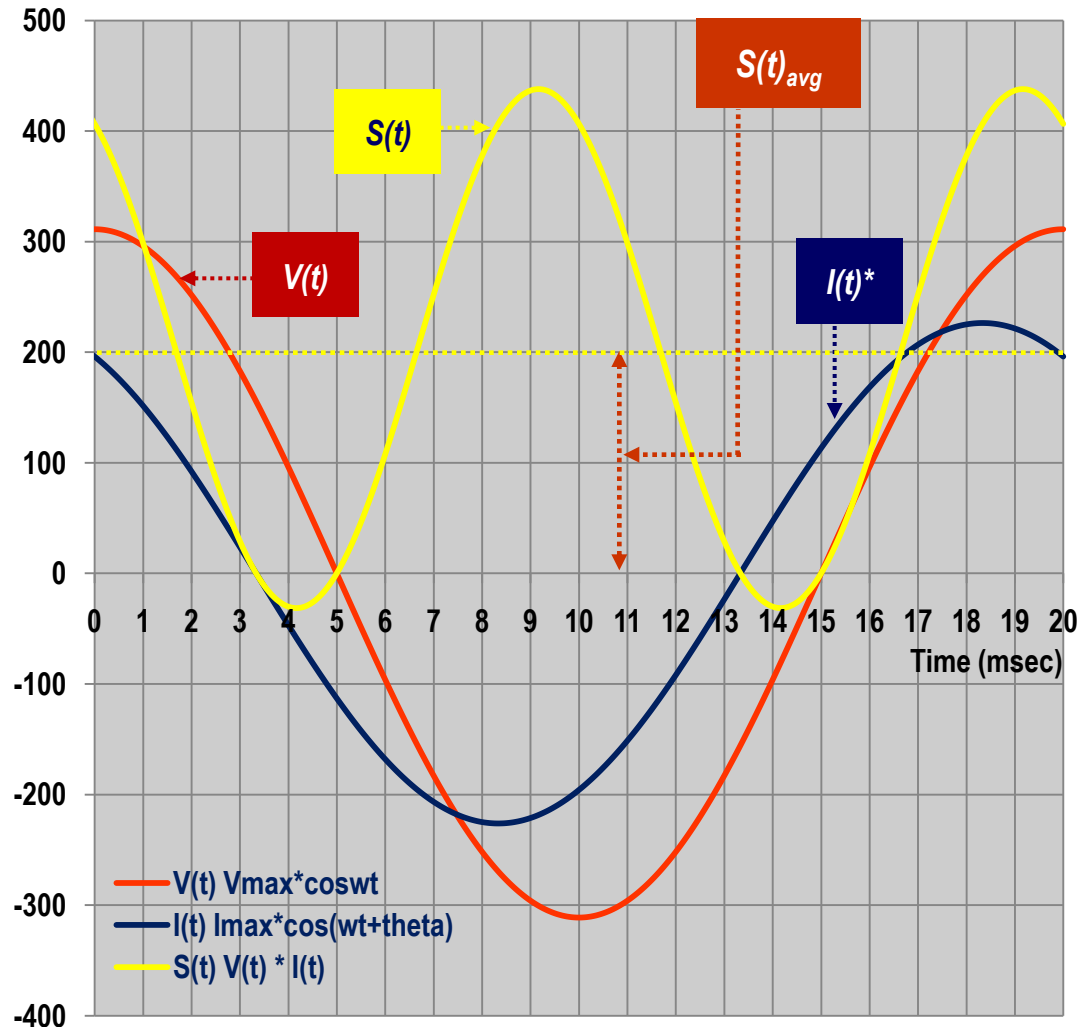
$$V_{max} = 100 \times \sqrt{2} = 144.4 \text{ Volts}$$

$$\begin{aligned} I &= V_{max} \angle 0^\circ / Z \angle \theta \\ &= 144.4 \angle 0^\circ / 5 \angle 53.13^\circ \\ &= 28.8 \angle -53.13^\circ \text{ Amp} \end{aligned}$$

$$I_{rms} = I_{max} / \sqrt{2} = 28.8 / \sqrt{2} = 20 \text{ Amp}$$



Example



Example

Solution

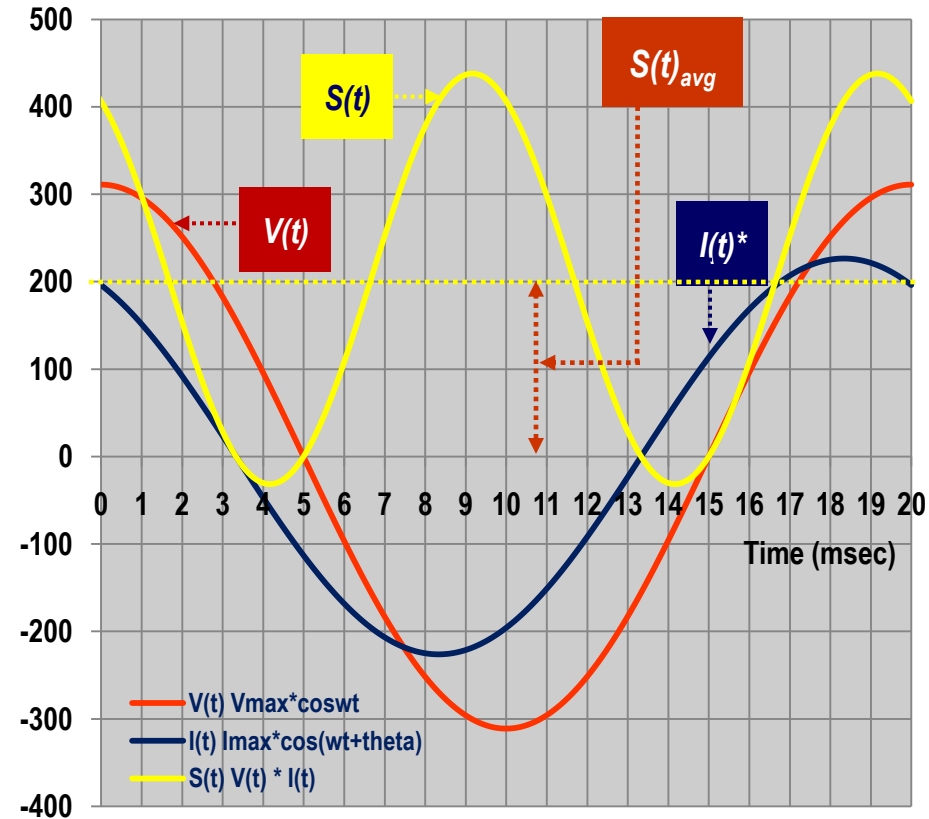
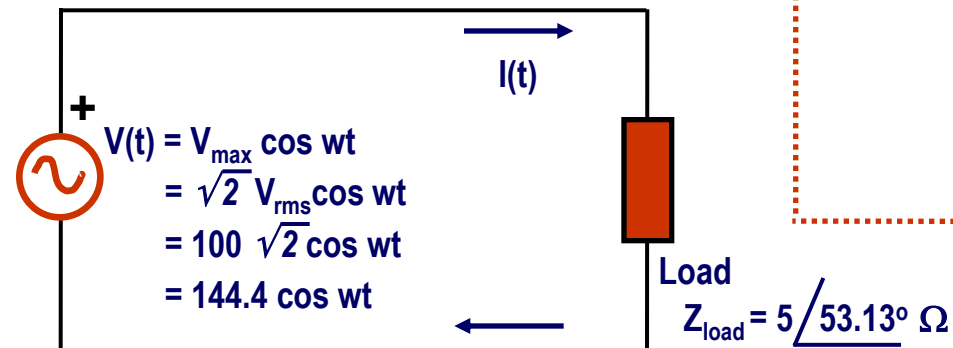
$$S(t)_{avg} = V_{rms} I_{rms} \cos \theta$$

$$= 100 \times 20 \cos 53.13 = 1200 \text{ Watt}$$

$$S(t) = V(t) I(t)$$

$$= \sqrt{2} \times 100 \cos wt \times \sqrt{2} \times 20 \cos (wt + 53.13^\circ)$$

$$= 4000 \cos wt \times \cos (wt + 53.13^\circ)$$



Please note that;
 “-” sign here has been changed to “+” due to the conjugate operation in the definition of power:
 $S = V \times I^*$

Example

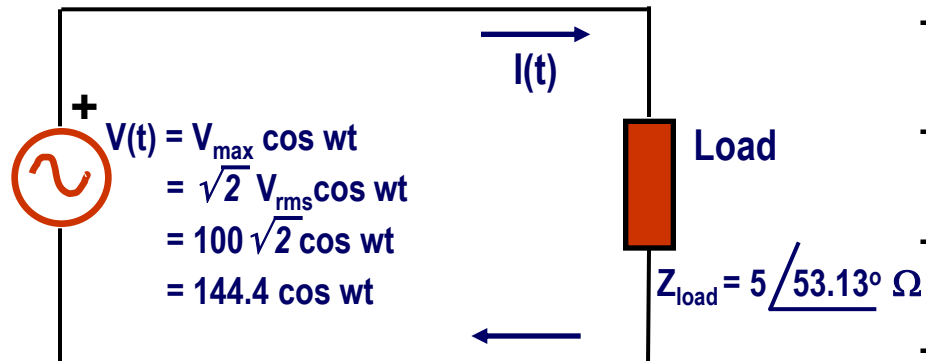
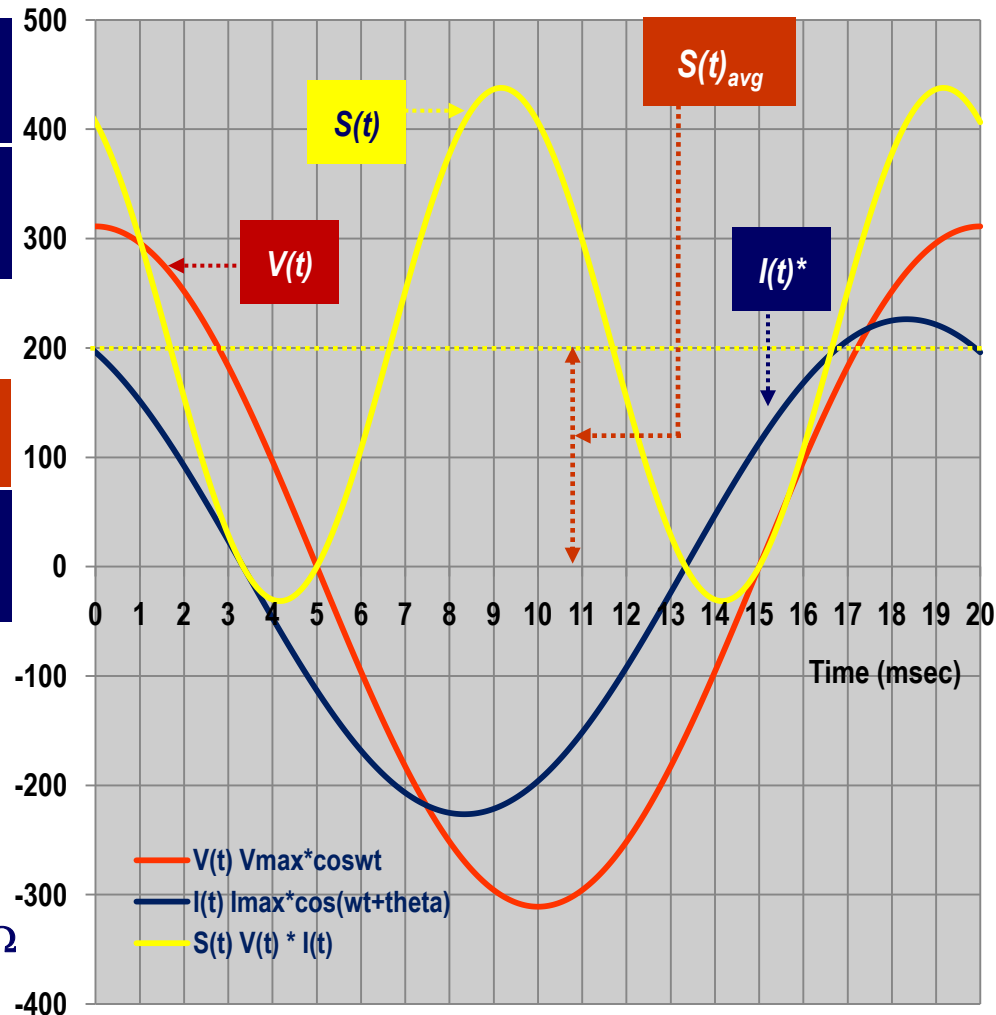
Solution

$$S(t) = 4000 \cos wt \times \cos (wt + 53.13^\circ)$$

or by using the following identity;

$$\cos a \cos b = \frac{1}{2} [\cos (a + b) + \cos (a - b)]$$

$$S(t) = 2000 [\cos (2wt + 53.13^\circ) + \cos 53.13^\circ]$$



Complex Power

Active Power Expression

Expanding the first term in the power expression;

$$S(t) = V_{rms} I_{rms} [\cos(2\omega t + \theta) + \cos \theta]$$

$$= V_{rms} I_{rms} (\cos 2\omega t \cos \theta - \sin 2\omega t \sin \theta + \cos \theta)$$

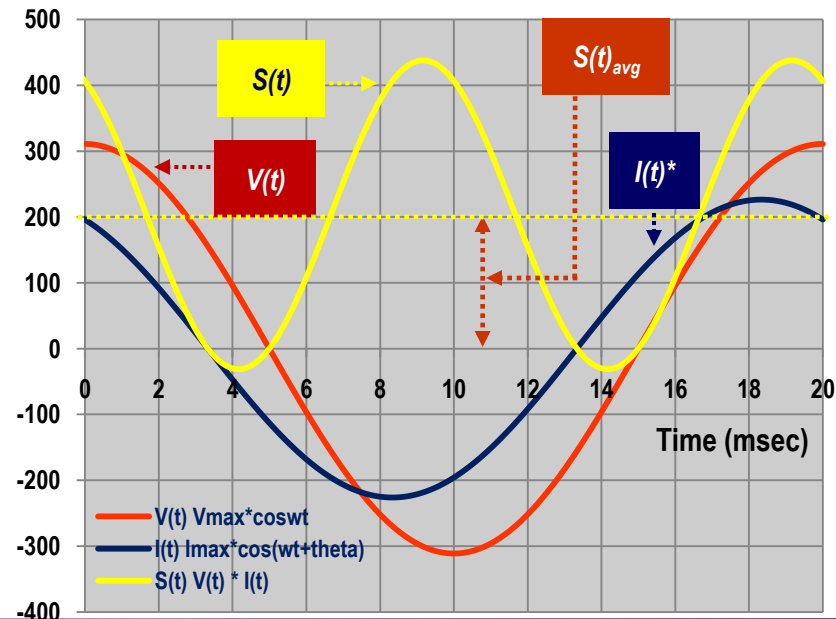
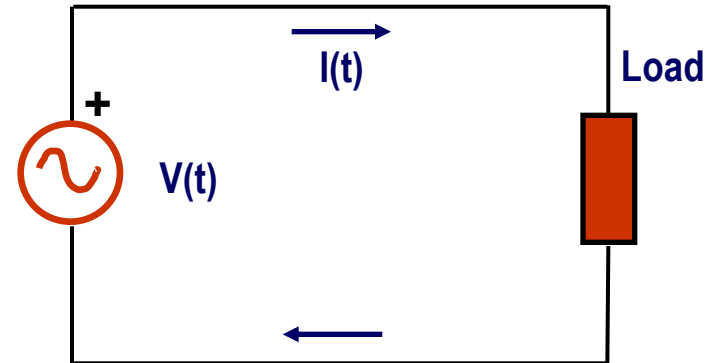
$$\cos(a + b) = \cos a \cos b - \sin a \sin b$$

and recombining the cosine terms;

$$= V_{rms} I_{rms} [\cos \theta (1 + \cos 2\omega t) - \sin 2\omega t \sin \theta]$$

$$P(t) = \text{Active power}$$

$$Q(t) = \text{Reactive power}$$



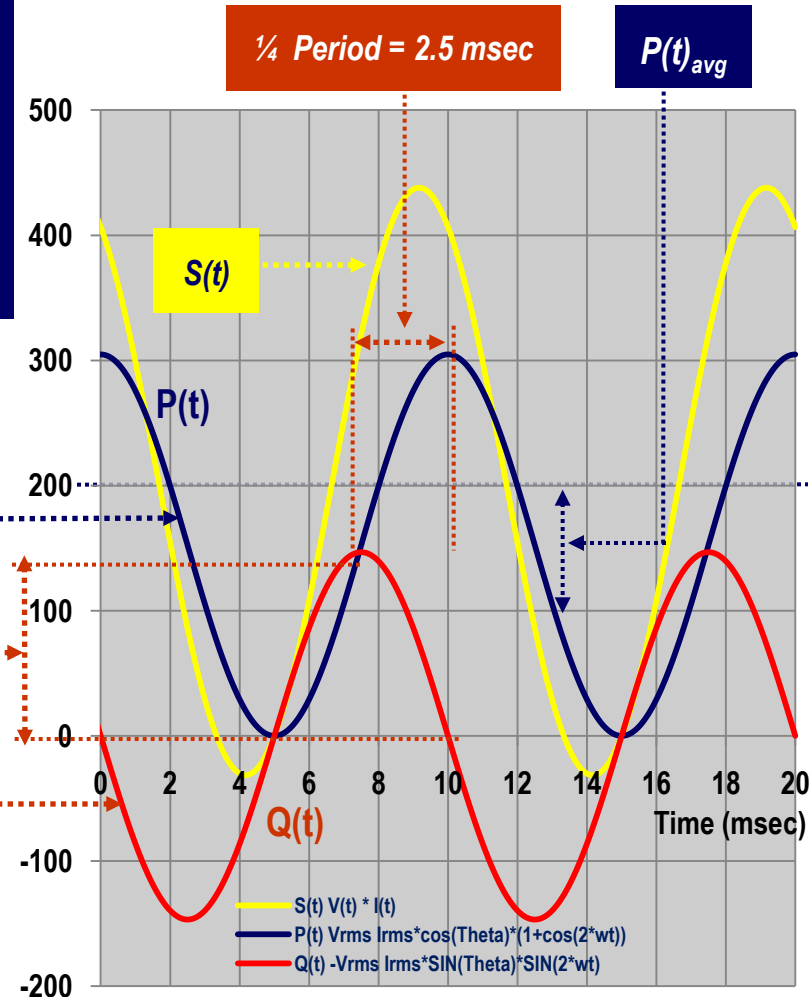
Complex Power

$$\begin{aligned}
 S(t) &= V_{rms} I_{rms} [\cos\theta (1 + \cos 2\omega t) - \sin 2\omega t \sin\theta] \\
 &= V_{rms} I_{rms} \cos\theta (1 + \cos 2\omega t) - \underbrace{V_{rms} I_{rms} \sin\theta}_{Q_{max}} \sin 2\omega t \\
 &= V_{rms} I_{rms} \cos\theta (1 + \cos 2\omega t) - Q_{max} \sin 2\omega t
 \end{aligned}$$

$P(t)$ = Active power

$$Q_{max} = V_{rms} I_{rms} \sin\theta$$

$Q(t)$ = Reactive power



Active and Reactive Powers – Summary

$$S(t) = \underbrace{V_{rms} I_{rms} \cos \theta}_{\text{Active power}} (1 + \cos 2\omega t) - \underbrace{V_{rms} I_{rms} \sin \theta \sin 2\omega t}_{\text{Reactive power}}$$

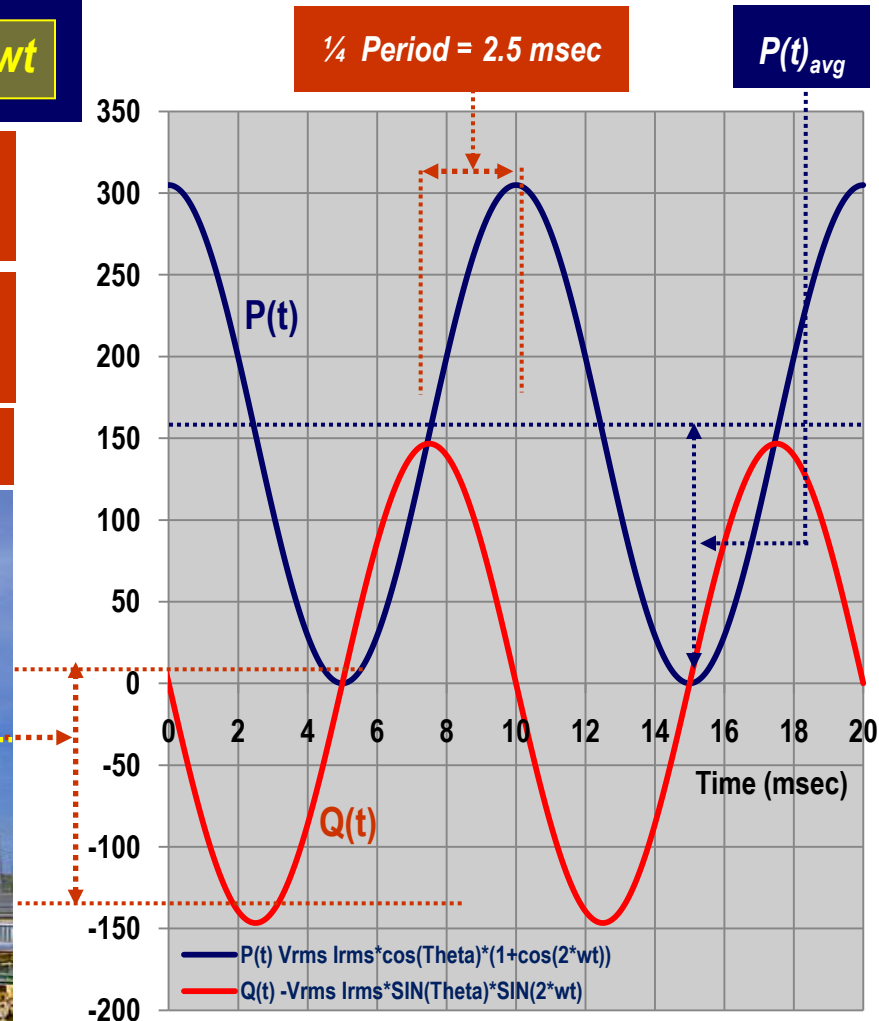
Active power

$$P(t)_{avg} = V_{rms} I_{rms} \cos \theta$$

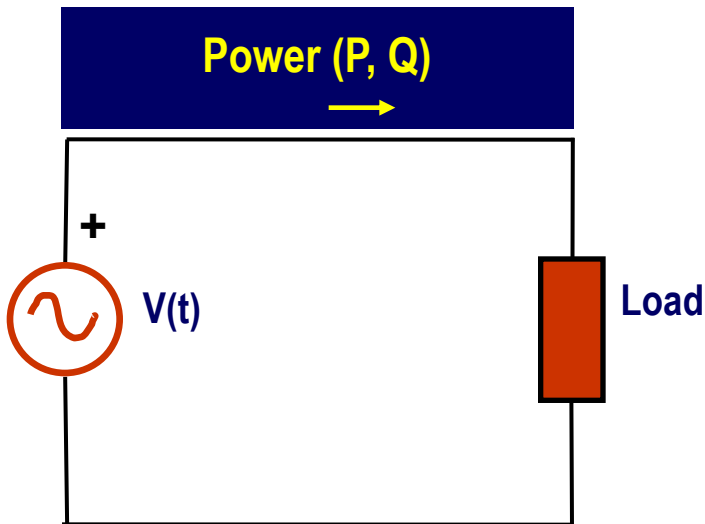
Reactive power

$$Q(t) = -Q_{max} \sin 2\omega t$$

Marmara, Unimar Power Plant 470 MW



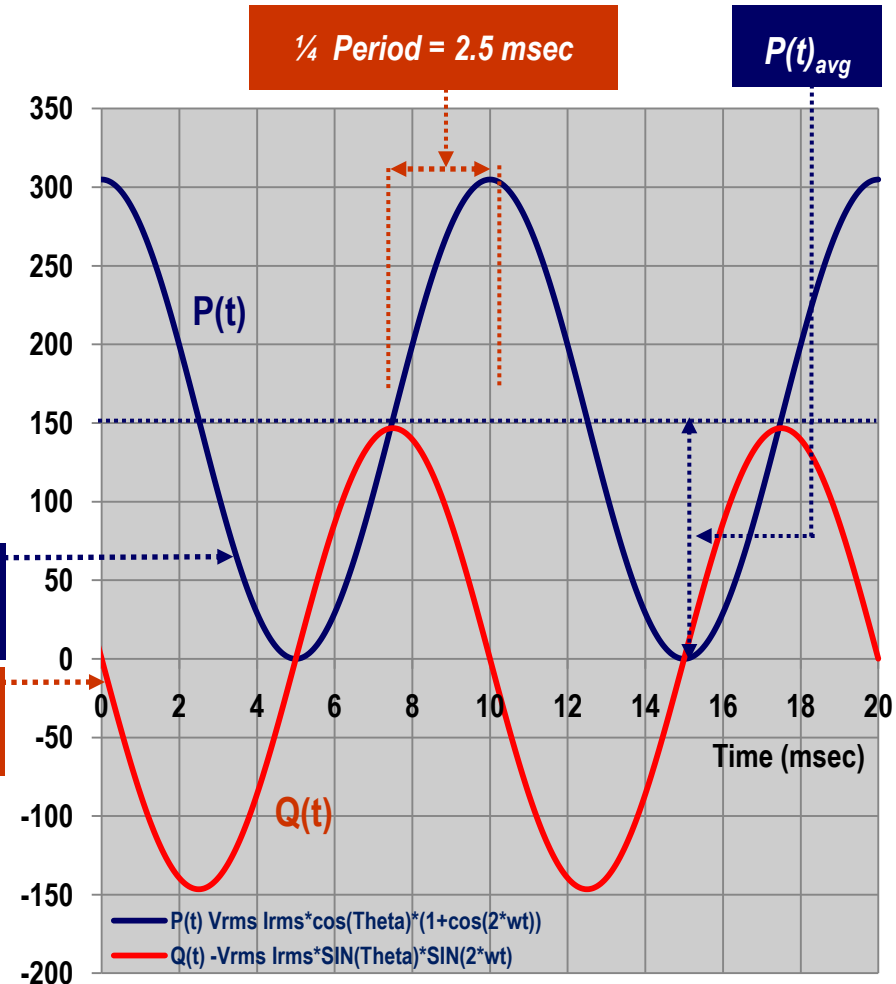
AC Power Active and Reactive Power Waveforms



Full period = 10 msec
 $\frac{1}{4}$ period = 2.5 msec
 $\frac{1}{4}$ period = $360^\circ / 4 = 90^\circ$

$P(t)$ = Active power

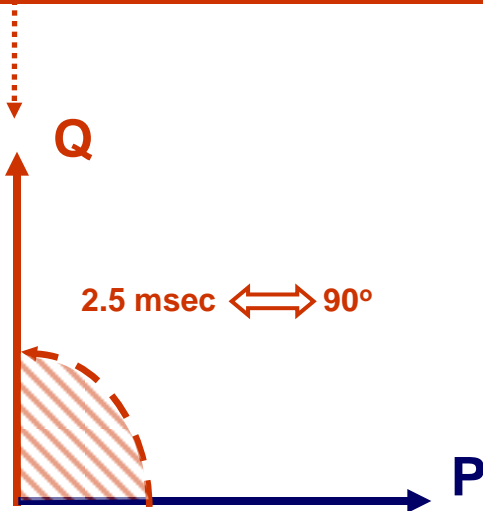
$Q(t)$ = Reactive power



AC Power Active and Reactive Power Waveforms

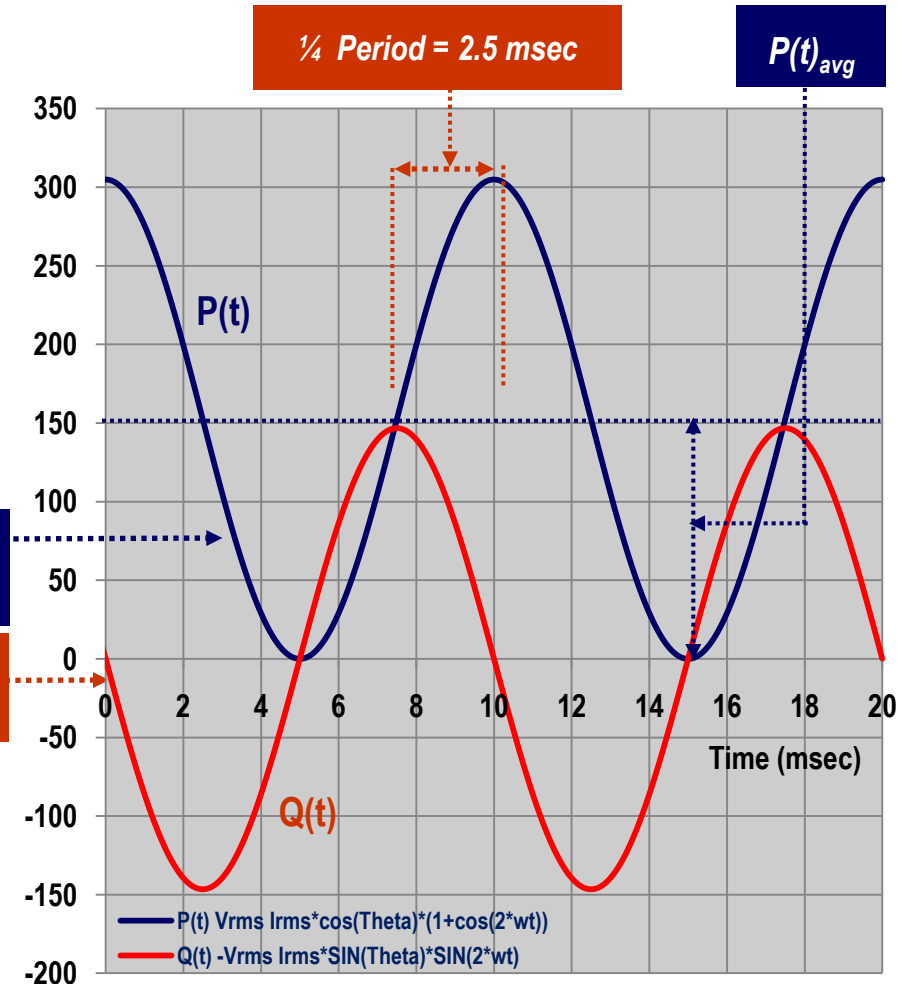
One revolution = 10 msec
Hence,
 $2.5 \text{ msec} = 360^\circ / 4 = 90^\circ$

Please note that Q leads P by 90°



$P(t)$ = Active power

$Q(t)$ = Reactive power



AC Power Active Power Waveform

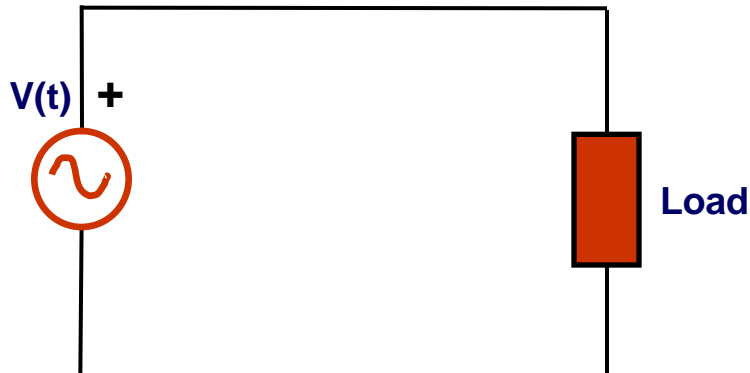
$$P(t) = V_{rms} I_{rms} \cos \theta (1 + \cos 2\omega t)$$

$$= \underbrace{V_{rms} I_{rms} \cos \theta}_{P(t)_{avg}} + \underbrace{V_{rms} I_{rms} \cos \theta \cos 2\omega t}_{P(t)_{sinusoidal}}$$

$P(t)_{avg}$

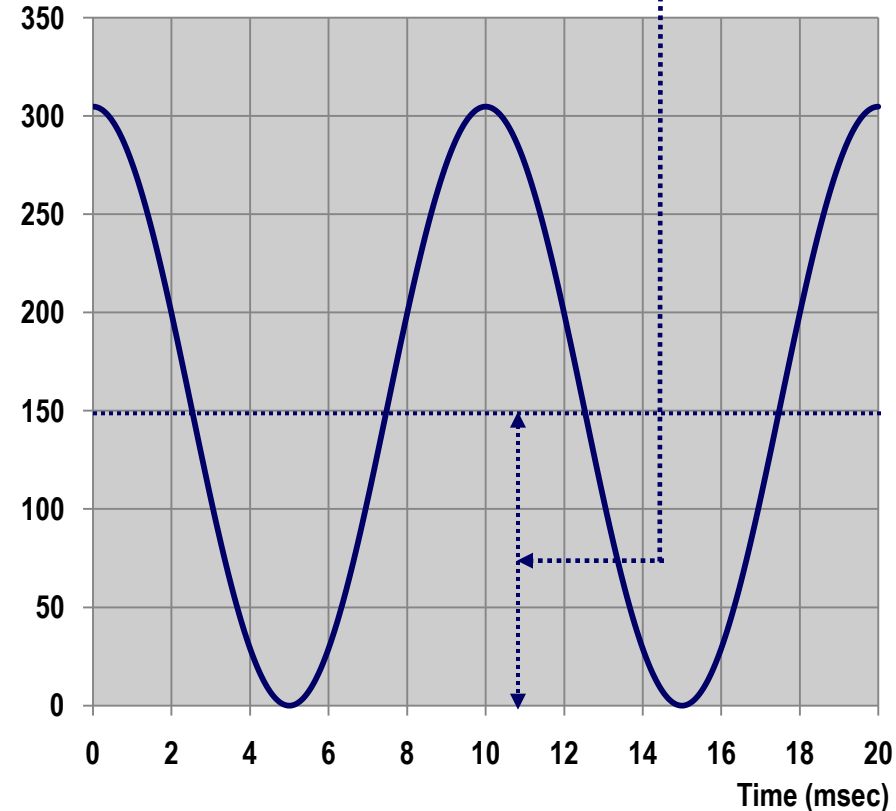
$P(t)_{sinusoidal}$

Active Power (P)



$$P(t)_{avg} = 150 \text{ W}$$

$P(t)$ = Active Power (Watt)



AC Power Reactive Power Waveform

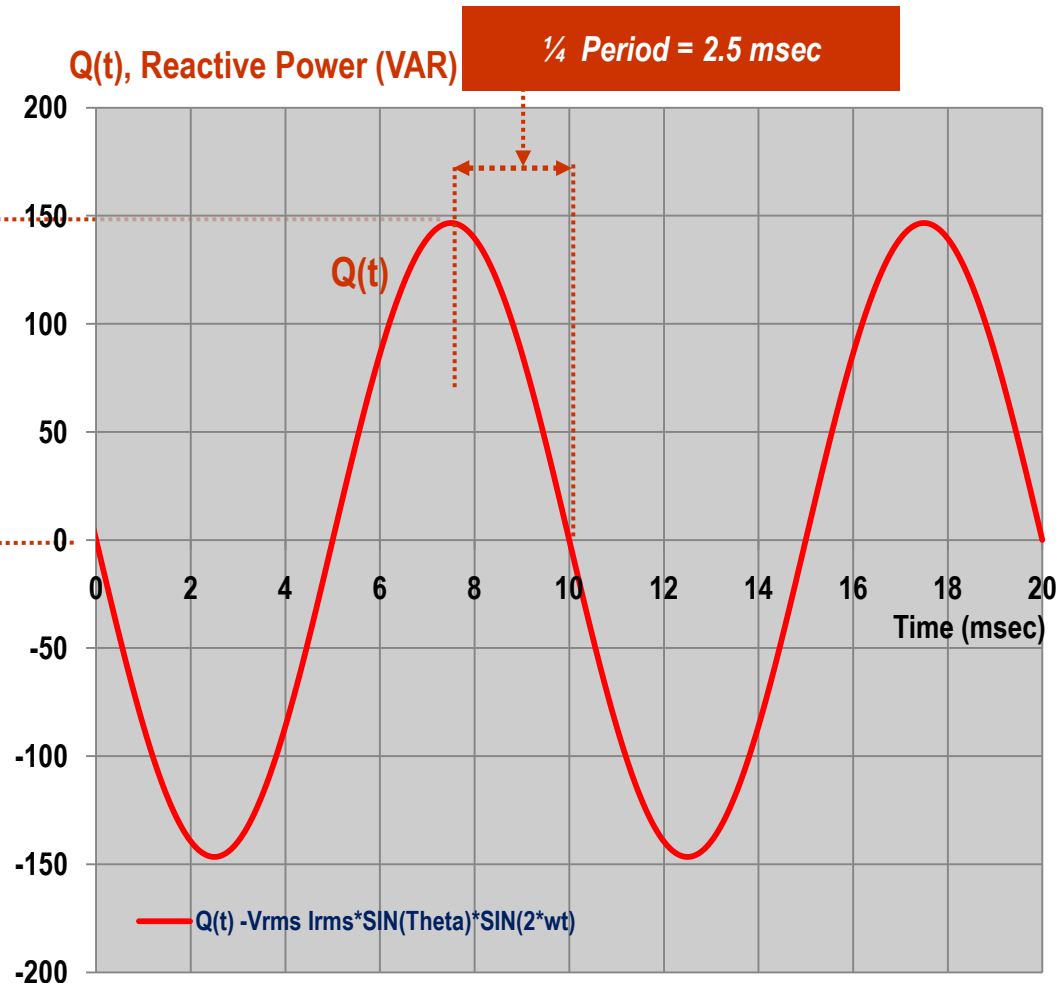
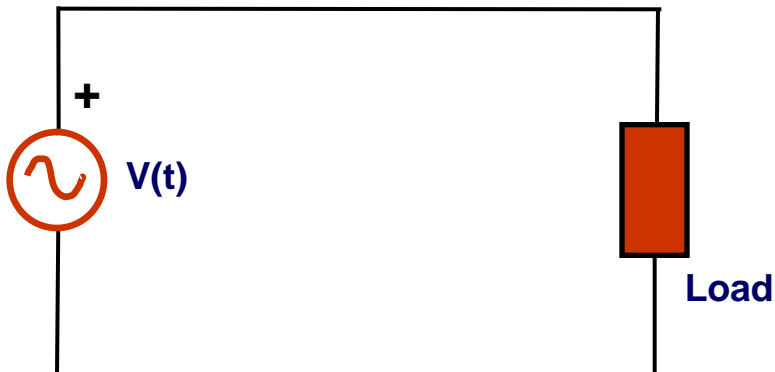
$$Q(t) = V_{rms} I_{rms} \sin \theta \times \sin 2\omega t$$

$$= Q_{max} \sin 2\omega t$$

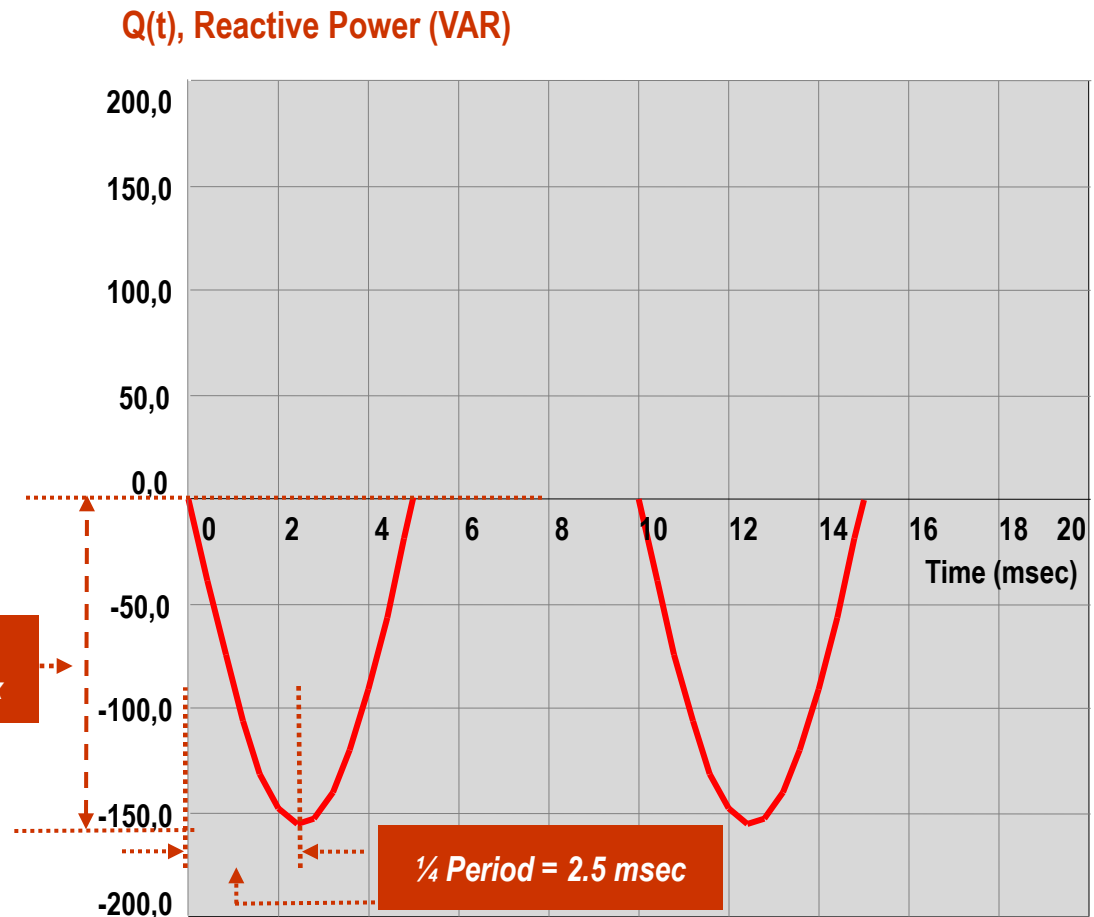
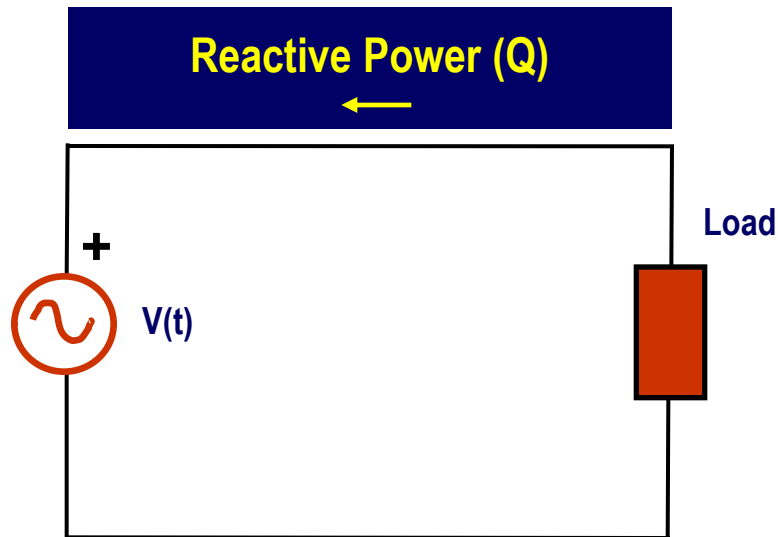
$Q(t)$ sinusoidal

Q_{max}

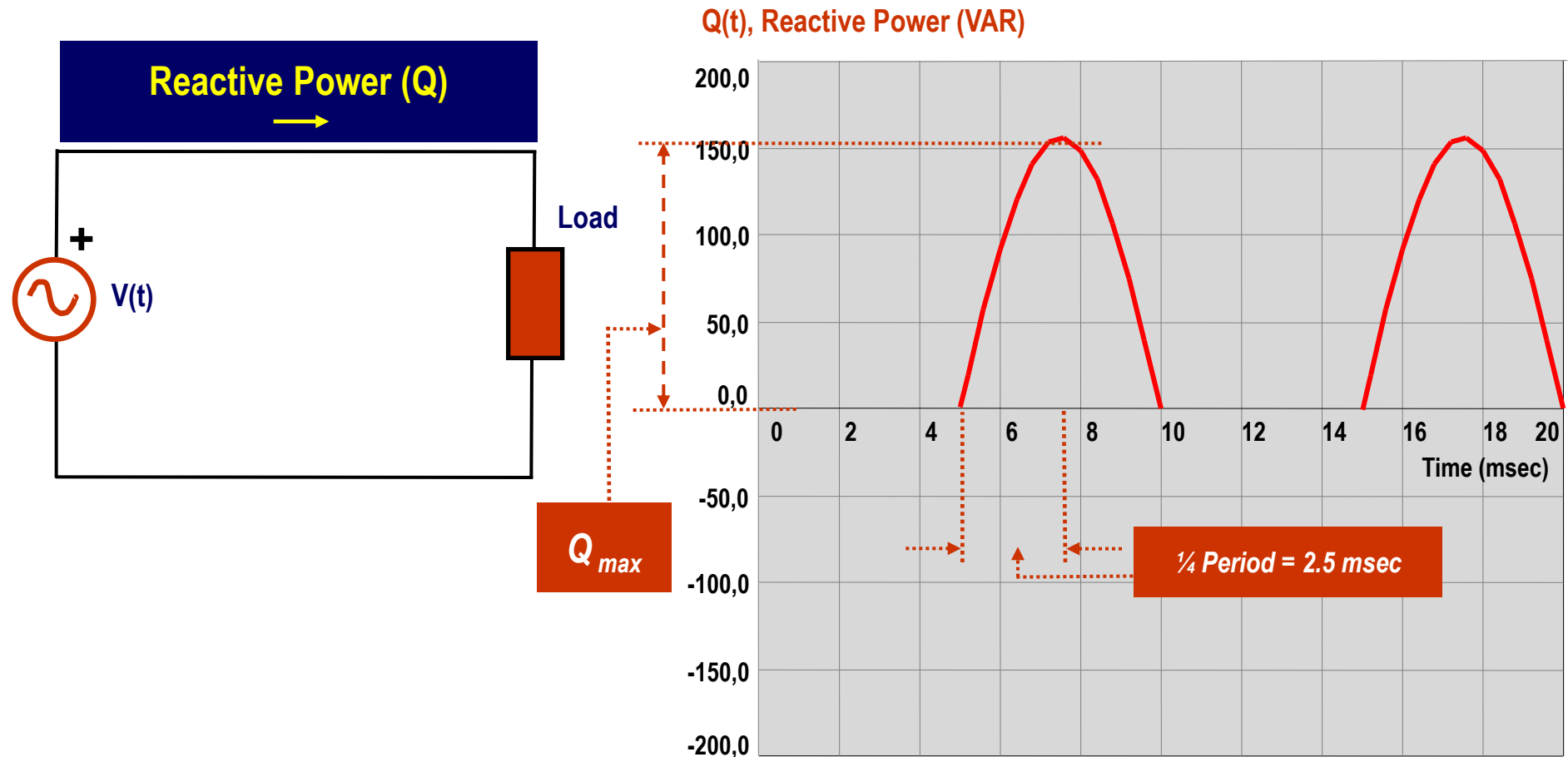
Reactive Power (Q)



AC Power Reactive Power Waveform (During the first 5 mseconds)



AC Power Reactive Power Waveform (During the next 5 mseconds)

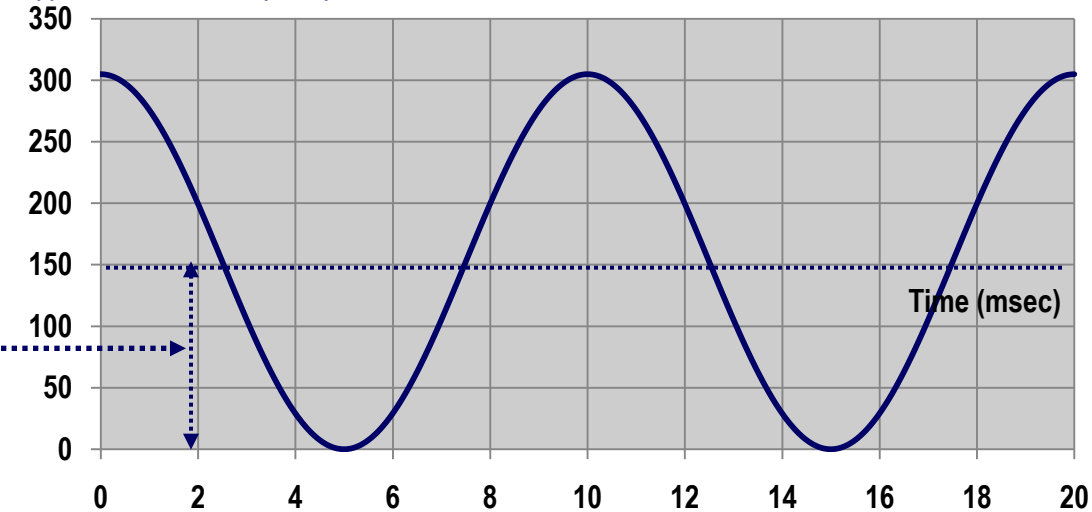


Phosors Representation of Active and Reactive Powers

Mean of $P(t)$ is called active power
Peak of $Q(t)$ is called reactive power

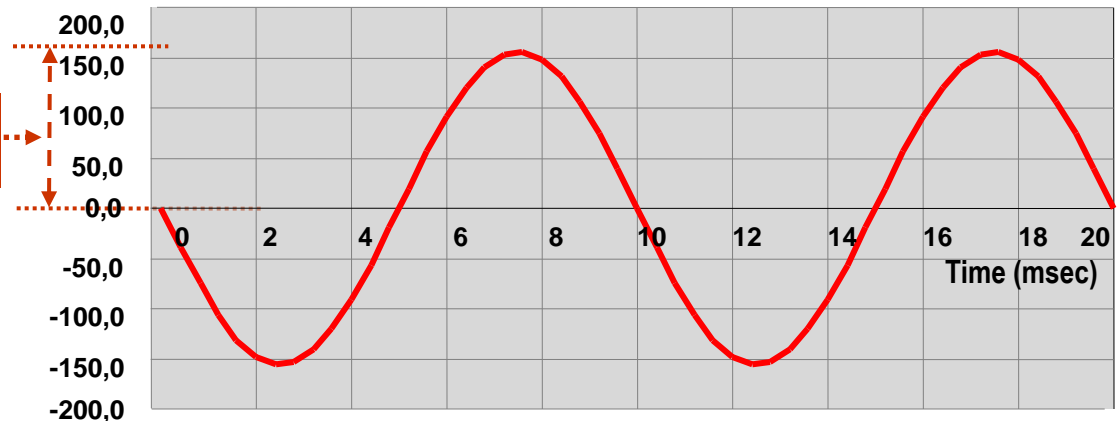
$$P(t)_{avg} = 150 \text{ W}$$

$P(t)$ = Active Power (Watt)



$$Q_{max} = 160 \text{ VAR}$$

$Q(t)$, Reactive Power (VAR)



Phosors Representation of Active and Reactive Powers

Voltage and Current

Angular speed: $w = 2\pi f$
 $= 2 \times 3.14 \times 50 = 314 \text{ rad/sec}$

Time for one revolution $= 1/f = 1/50 = 0.020 \text{ sec}$
 $= 20 \text{ msec}$

Hence,

Angle for $\frac{1}{4}$ revolution $= 360^\circ / 4 = 90^\circ$

Time for $\frac{1}{4}$ revolution $= 20 \text{ msec} / 4 = 5 \text{ msec}$

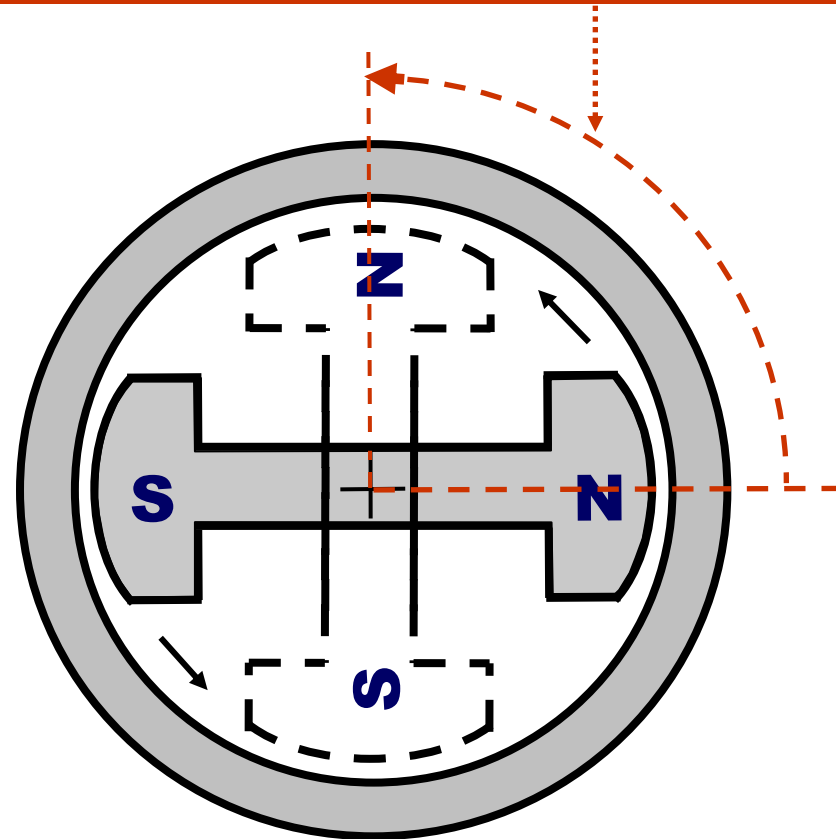
Active and Reactive Power

Angular speed: $w' = 2w = 4\pi f$
 $= 2 \times 314 = 628 \text{ rad/sec}$

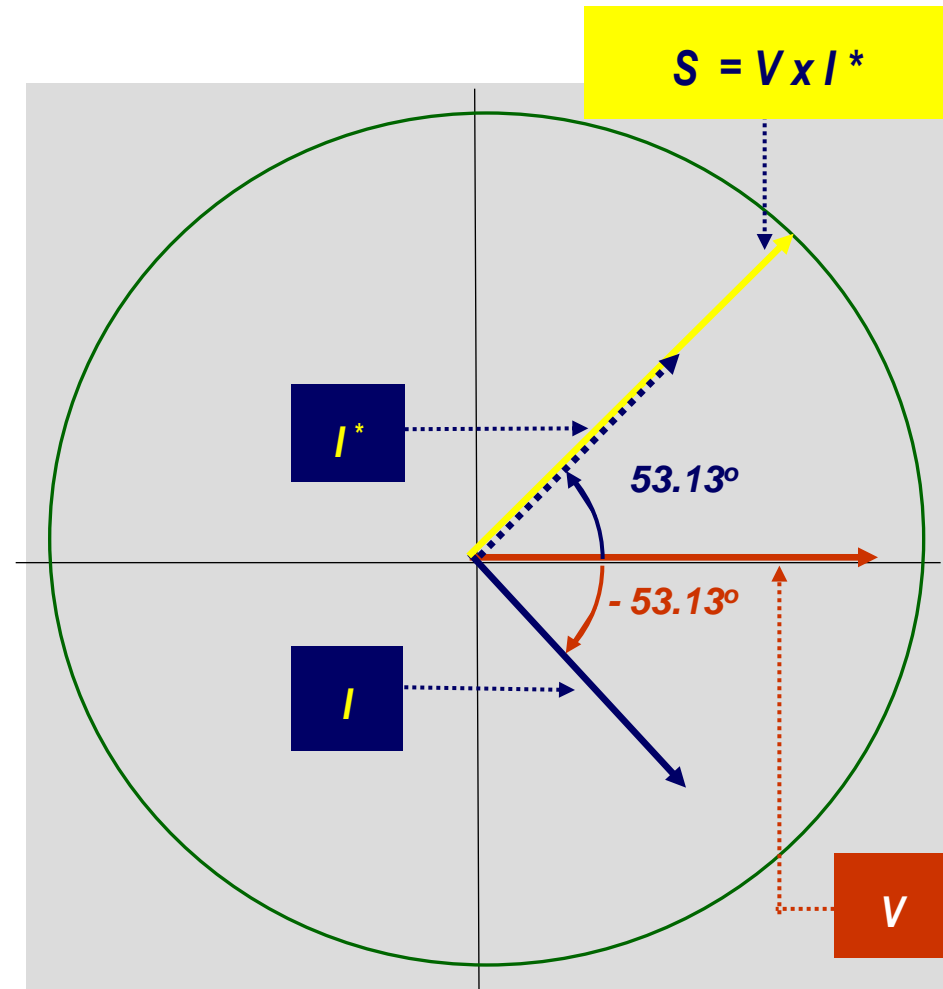
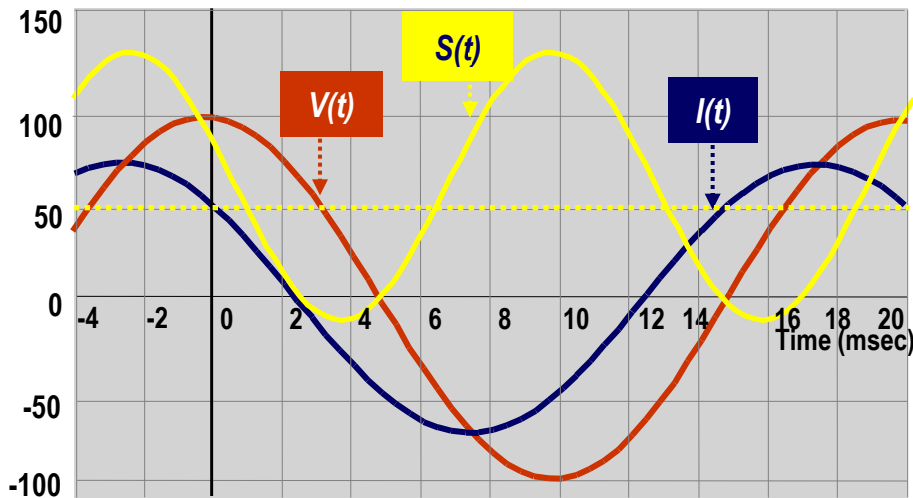
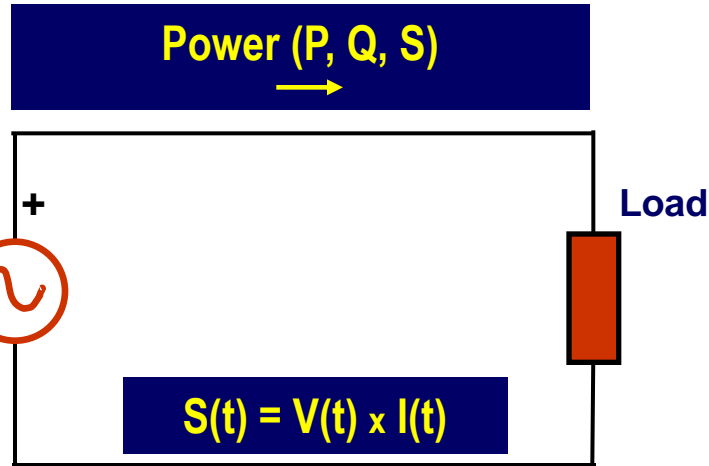
Time for one revolution $= 10 \text{ msec}$

Time for $\frac{1}{4}$ revolution $= 10 \text{ msec} / 4 = 2.5 \text{ msec}$

Angle $= 90^\circ$, Time for $\frac{1}{4}$ revolution $= 20/4 = 5 \text{ msec}$

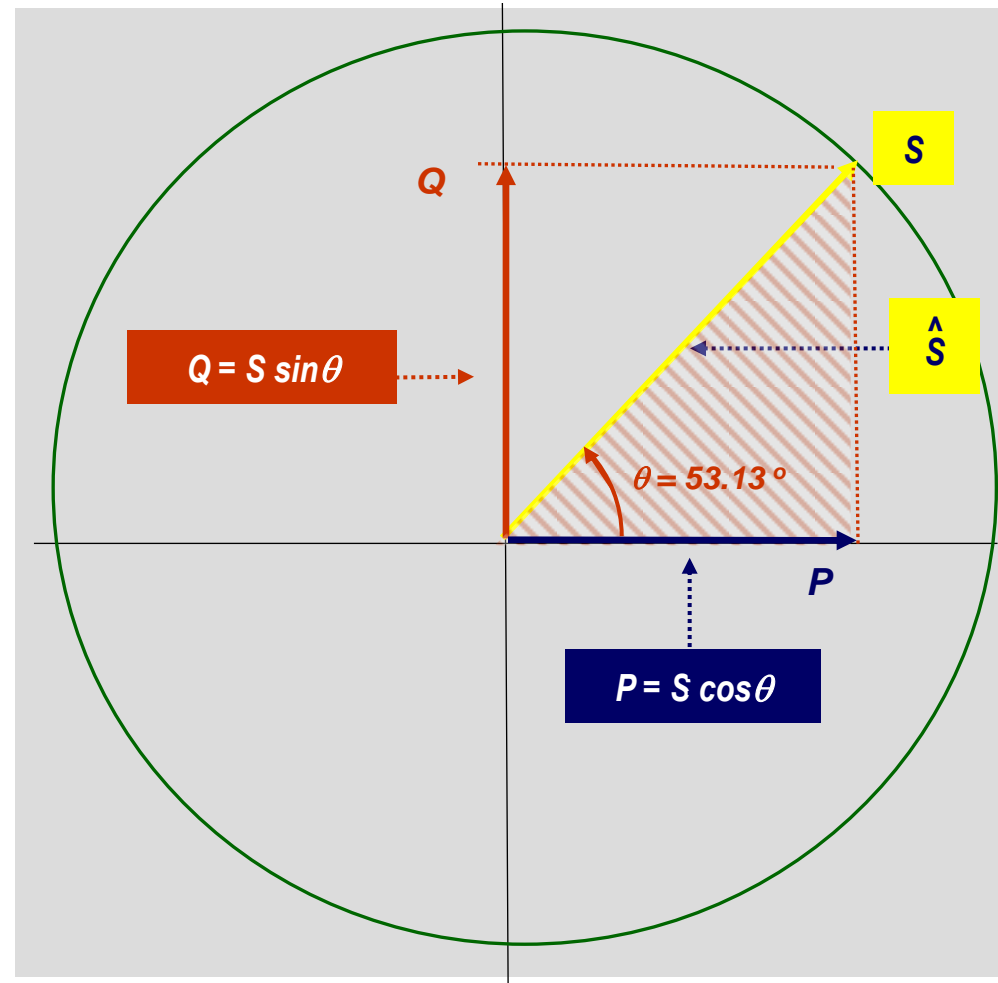
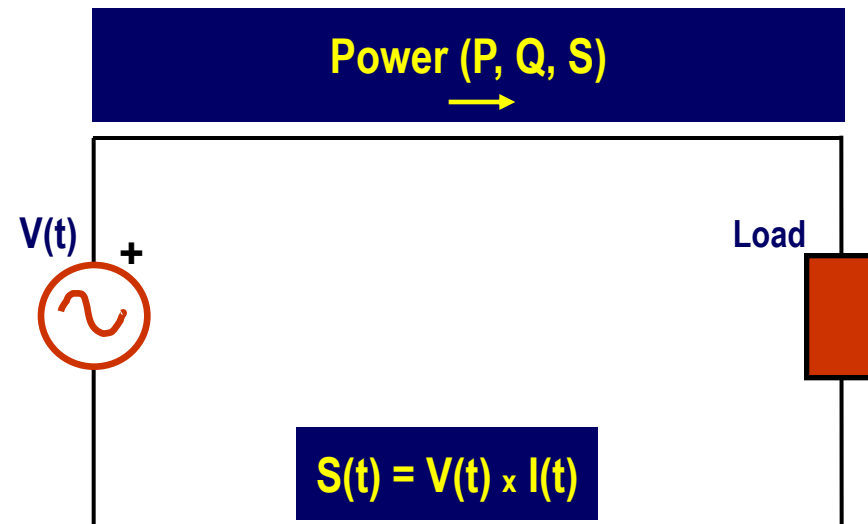


Phosors Representation of Active and Reactive Powers



Phosors Representation of Active and Reactive Powers

| | |
|----------------|-------------------------------------|
| Total power | $ S = V_{rms} I_{rms}$ |
| | $ S = \sqrt{P^2 + Q^2}$ |
| Active power | $ P = V_{rms} I_{rms} \cos \theta$ |
| Reactive power | $ Q = V_{rms} I_{rms} \sin \theta$ |



Phosors Representation of Active and Reactive Powers

S - Total power

(k) VA (kVA)

P- Active power

(k) Watt (kW)

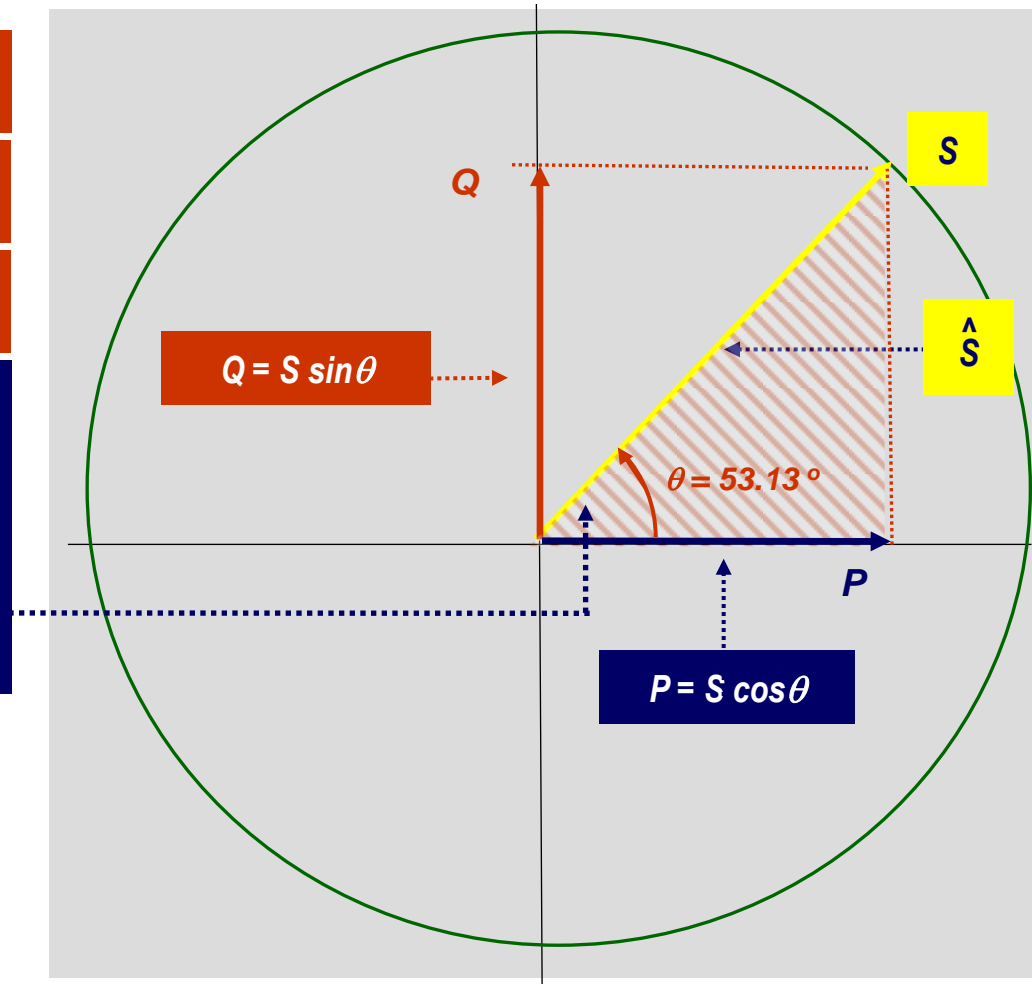
Q - Reactive power

(k) VAR (kVAR)

Please note that this angle depends only on the resistance R and reactance X of the load, i.e.

$$\theta = \tan^{-1} X / R$$

$$= \tan^{-1} Q / P$$



Basic Conversions

Polar Representation

$$S \angle \theta$$

Please note that this angle depends only on the resistance R and reactance X of the load

$$\theta = \tan^{-1} X / R$$

$$= \tan^{-1} Q / P$$

$$X / R = Q / P$$

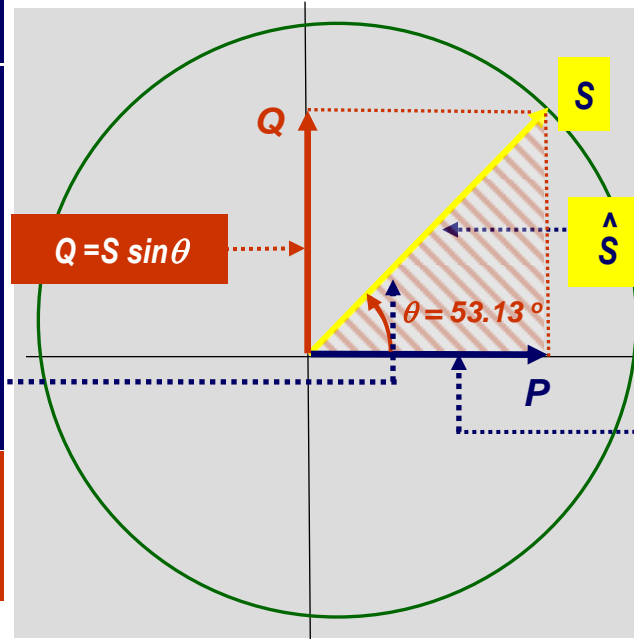
$$\text{i.e. if } X = 0 \rightarrow Q = 0$$

$$P = S \cos \theta, \quad Q = S \sin \theta$$

$$S = \sqrt{P^2 + Q^2}, \quad \theta = \tan^{-1} (Q / P)$$

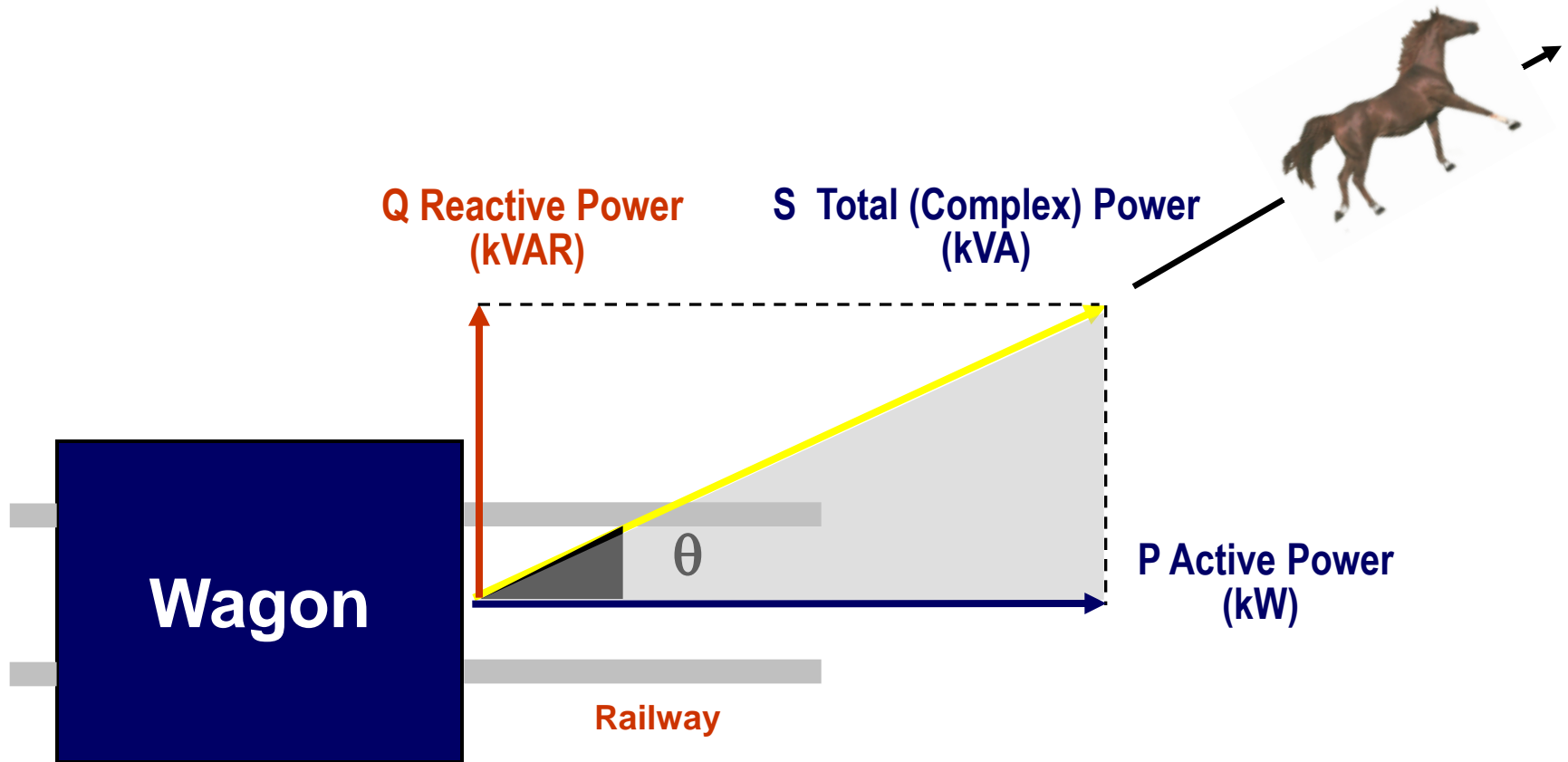
Rectangular Representation

$$P + jQ$$



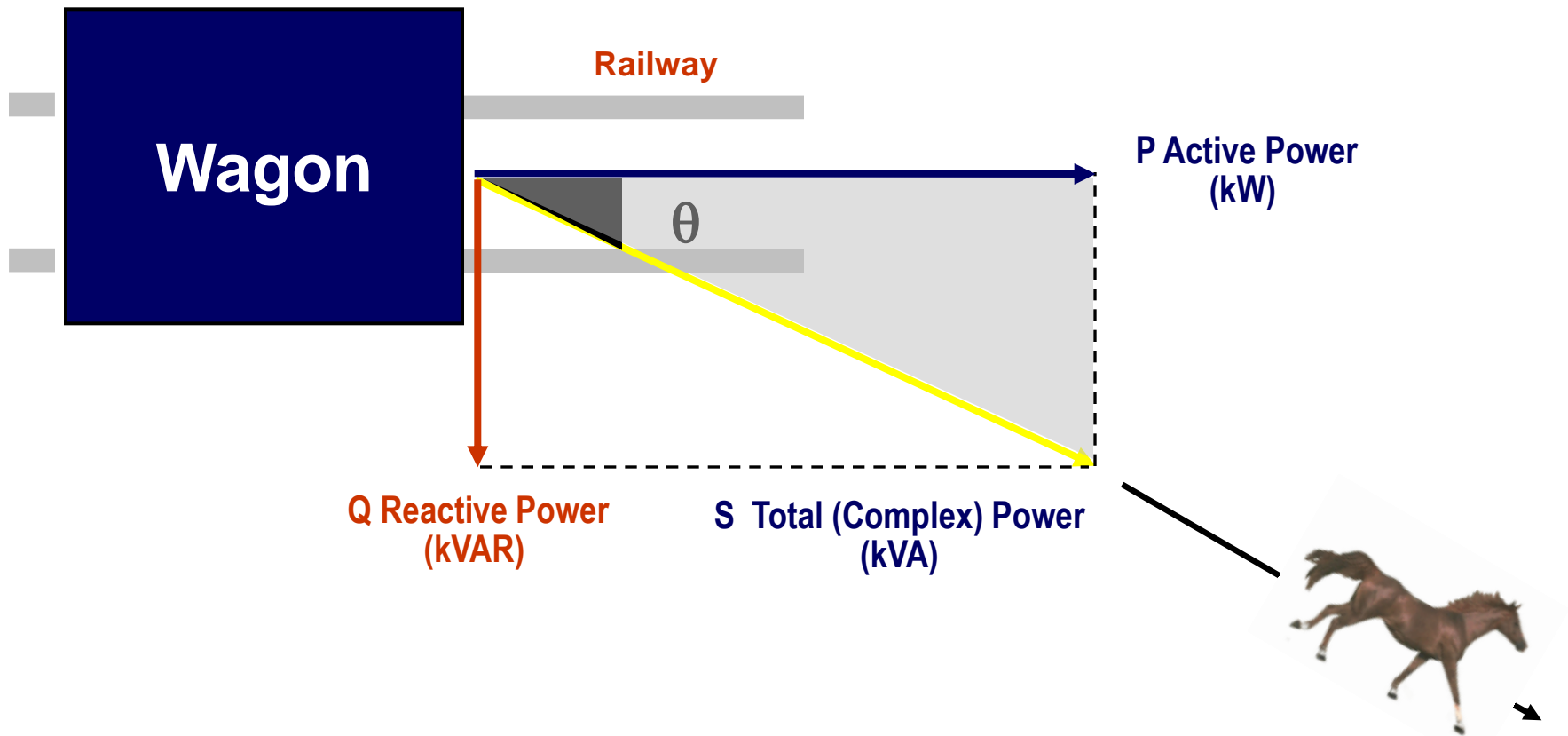
$$P = S \cos \theta$$

AC Power Active Reactive Powers (in the first 5 mseconds)

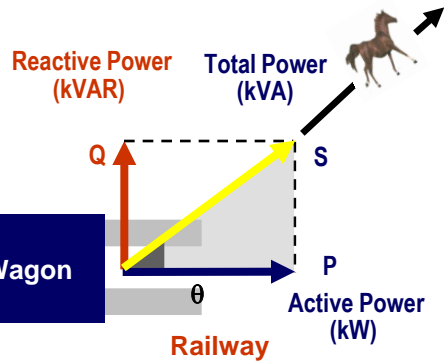


AC Power

AC Power Active Reactive Powers (in the next 5 mseconds)

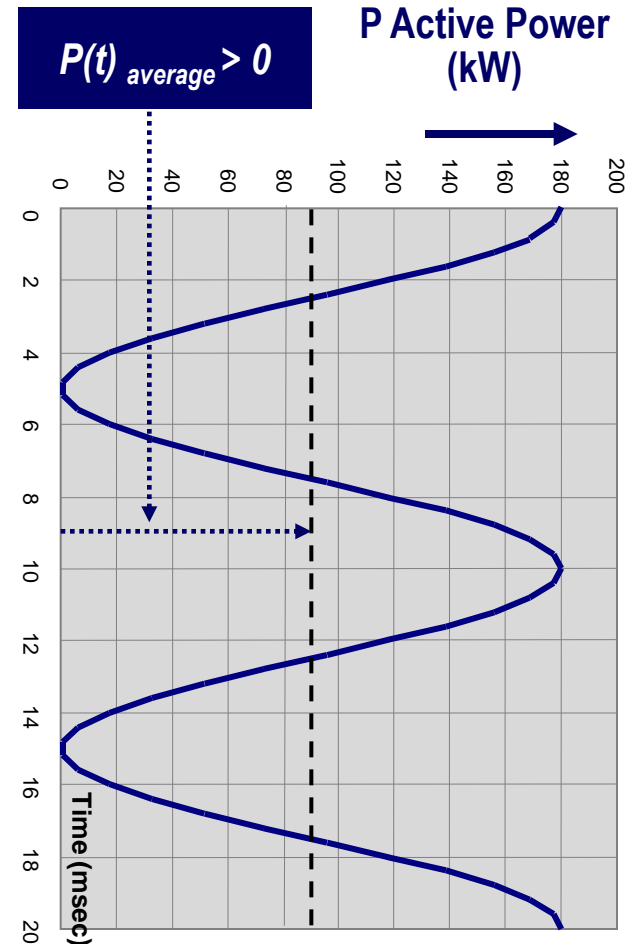
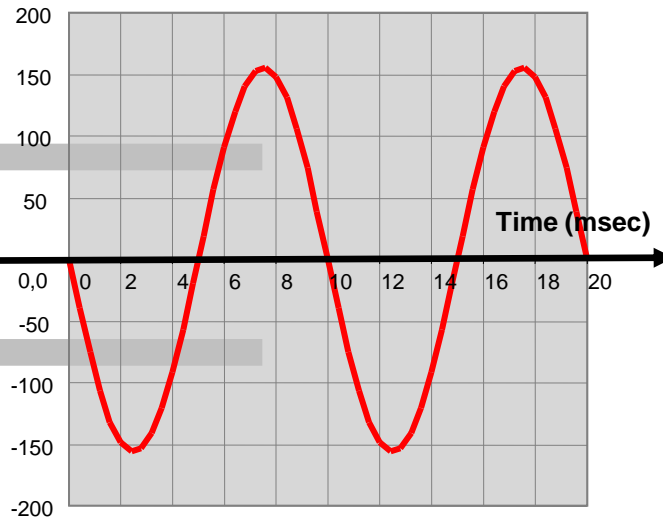


AC Power Active Reactive Powers



Q Reactive Power (kVAR)

Wagon



Active-Reactive Powers

Polar Representation

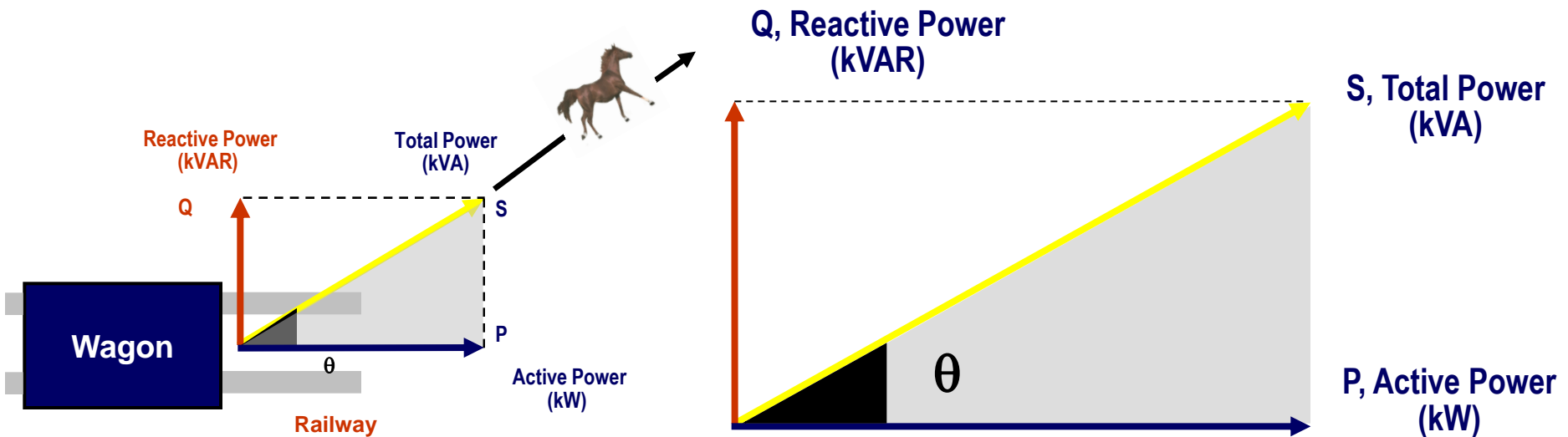
$$S \angle \theta$$

$$P = S \cos \theta, \quad Q = S \sin \theta$$

$$S = \sqrt{P^2 + Q^2}, \quad \theta = \tan^{-1}(Q / P)$$

Rectangular Representation

$$P + jQ$$



Active-Reactive Powers

Total power

$$|S| = V_{rms} I_{rms}$$

$$|S| = \sqrt{P^2 + Q^2}$$

Active power

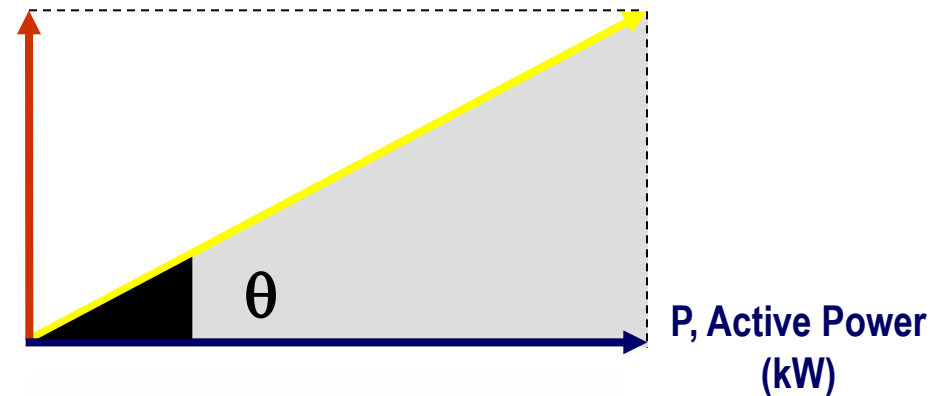
$$|P| = V_{rms} I_{rms} \cos \theta$$

Reactive power

$$|Q| = V_{rms} I_{rms} \sin \theta$$

Q, Reactive Power
(kVAR)

S, Total (Complex) Power
(kVA)



Reactive Power
(kVAR)

Total Power
(kVA)

Q

S

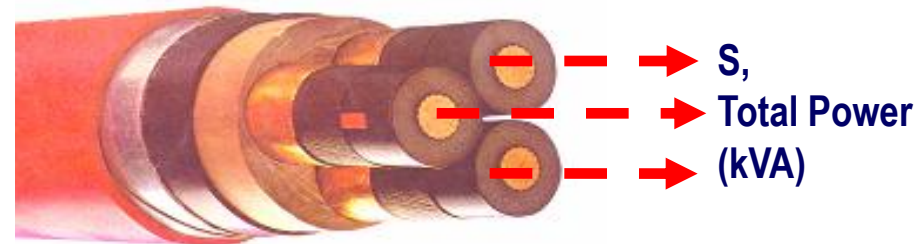
P

Active Power
(kW)

Wagon

Railway

θ



AC Power

Power Meters

Analog



Digital



Power Analyzer

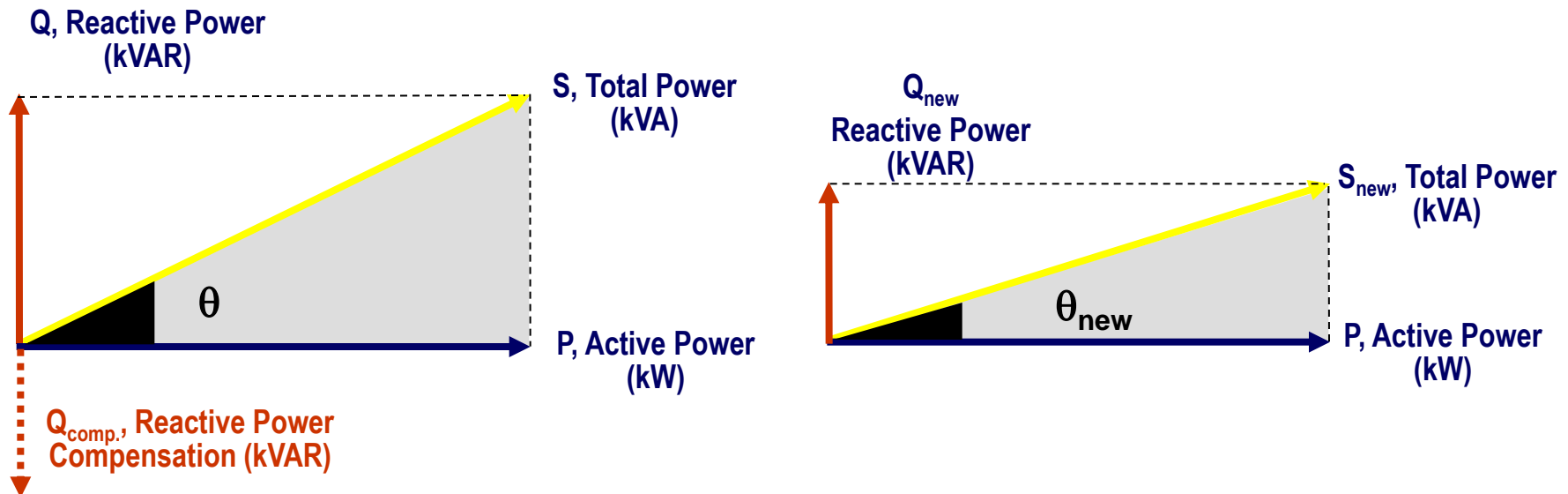


Clamp Type Current Transformers

Reactive Power Compensation

Definition

Reactive power compensation is partial or full cancellation of the reactive component of complex power by introducing a negative (compensation) component



Power Factor

Definition

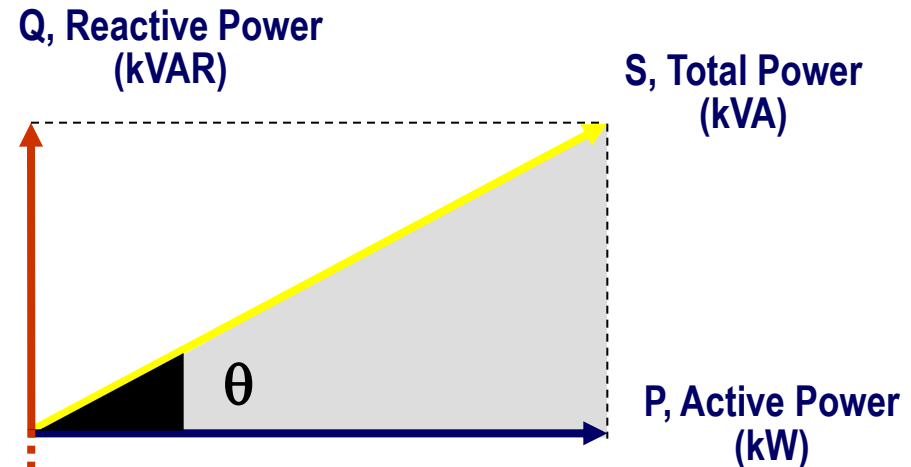
Cosine of the angle between S and P is called **Power Factor** of the load

$$\text{Power Factor} = \text{p.f.} = \cos \theta$$

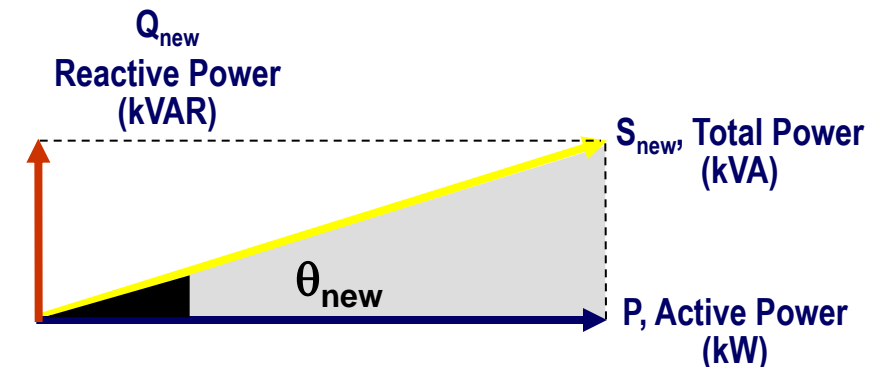
$$= \cos (\tan^{-1} Q / P)$$

Please note that reducing Q means reducing the angle θ , and hence increasing power factor

*Hence, reactive power compensation is sometimes called as “**Power Factor Correction**”, i.e. correcting power factor to a value near unity*



$Q_{\text{comp.}}$, Reactive Power Compensation (kVAR)



Full or Partial Compensation

Partial Compensation

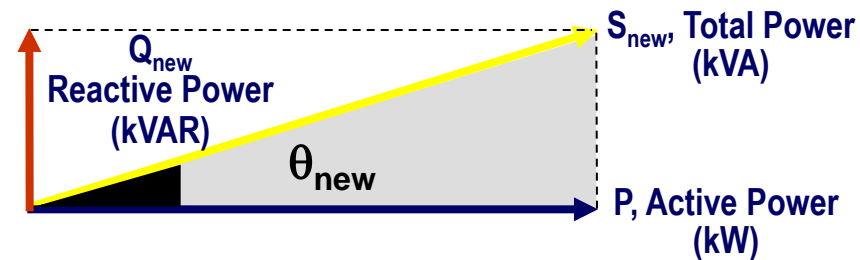
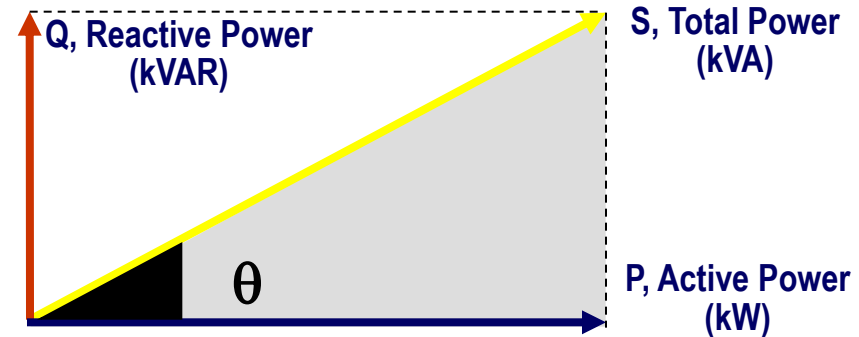
Partial compensation is the case, where **Power Factor** is raised to a value not reaching unity

$$\begin{aligned} \text{Power Factor}_{\text{new}} &= p.f._{\text{new}} = \cos \theta_{\text{new}} \\ &= \cos (\tan^{-1} Q_{\text{new}} / P) \end{aligned}$$

Full Compensation

Full compensation is the case, where **Power Factor** is unity

$$\begin{aligned} \text{Power Factor}_{\text{new}} &= p.f._{\text{new}} = \cos \theta_{\text{new}} \\ &= \cos (\tan^{-1} 0 / P) = 1 \end{aligned}$$



$$Q_{\text{new}} = 0$$

$$\theta_{\text{new}} = 0$$

$$S_{\text{new}} = P$$



Charging Principle Applied by TEDAS

If

$$|Q/P| > 1/3$$

Then, reactive power is charged

If

$$|Q/P| < 1/3$$

Then, reactive power is free

Please note that

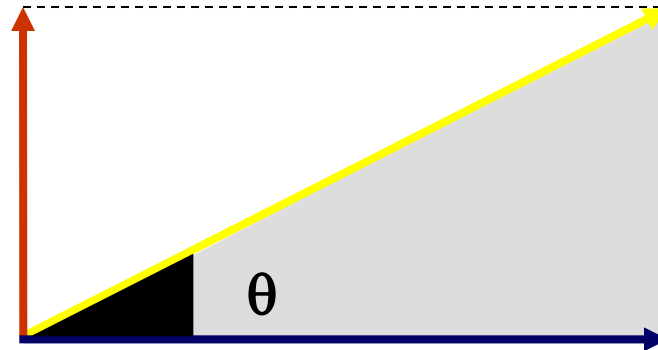
$$|Q/P| > 1/3$$

means;

$$\tan^{-1}(1/3) = 18.435^\circ$$

$$\cos 18.435^\circ = 0.949 \approx 0.95$$

Q, Reactive Power
(kVAR)



S, Total Power
(kVA)

P, Active Power
(kW)

Why Partial Compensation is Preferred ?

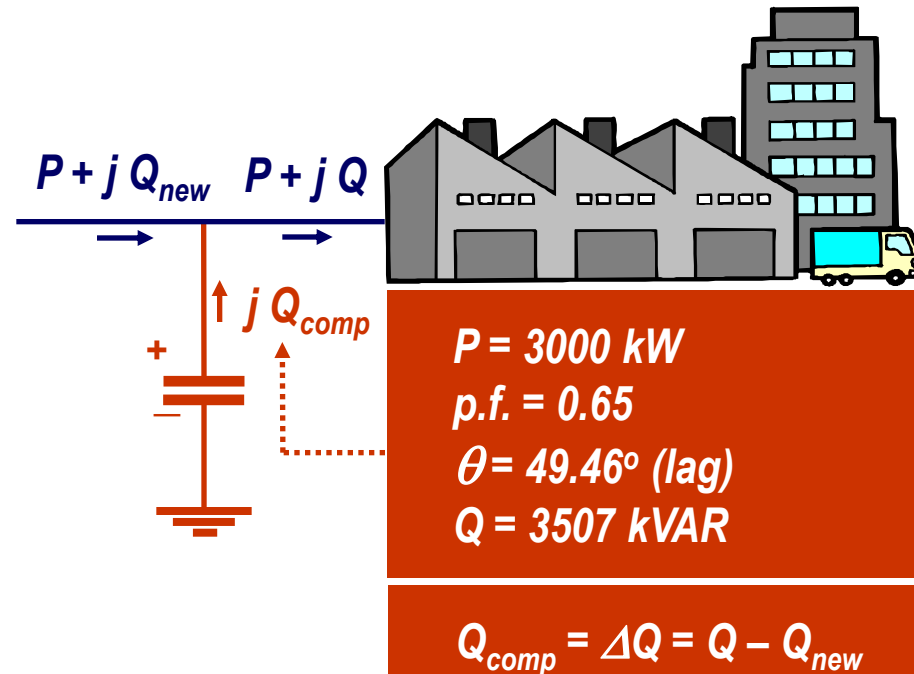
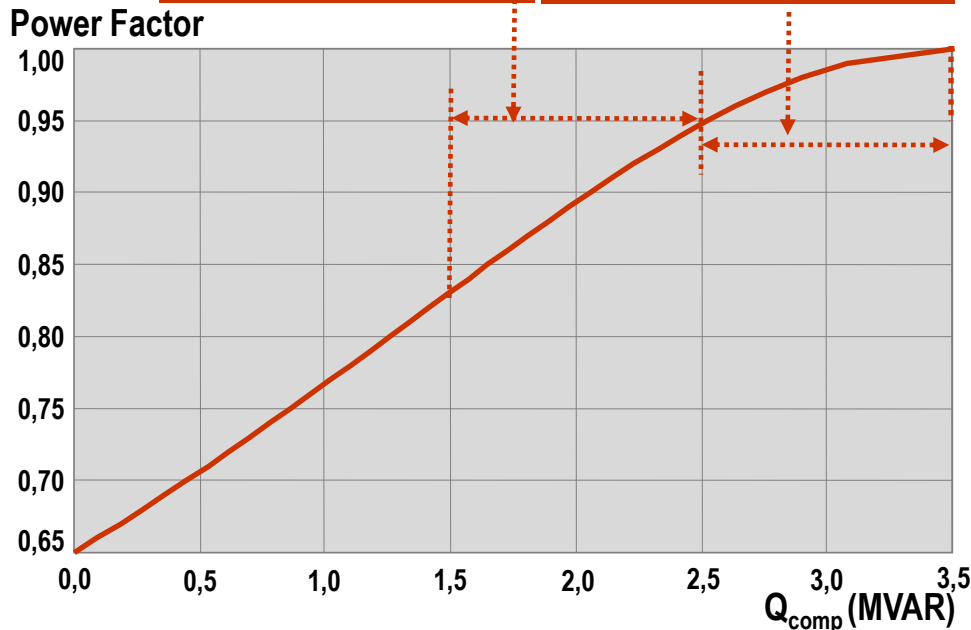
Partial Compensation

Due to economic reasons, full compensation is rarely implemented

Reactive power needed to raise p.f. from 0.95 to 1 is the same as that for raising p.f. from 0.83 to 0.95 (not worthwhile)

Reactive power needed to raise p.f. from 0.83 to 0.95

Reactive power needed to raise p.f. from 0.95 to unity



Application of Reactive Power Compensation

Reduction of Equipment Loading

- Transformers
- Lines
- Cables

are priced with respect to the power rating (kVA)

Prices of these equipments on the other hand, are determined by the cross-section (mm^2) of the equipment

| Cross Section (mm^2) | Current Capacity (Amp) |
|------------------------------------|---------------------------|
| 1.0 | 12.0 |
| 1.5 | 16.0 |
| 2.5 | 21.0 |
| 4.0 | 27.0 |
| 6.0 | 35.0 |
| 10.0 | 48.0 |
| 16.0 | 65.0 |
| 25.0 | 88.0 |
| 35.0 | 110.0 |
| 50.0 | 140.0 |
| 70.0 | 175.0 |
| 95.0 | 215.0 |
| 120.0 | 225.0 |

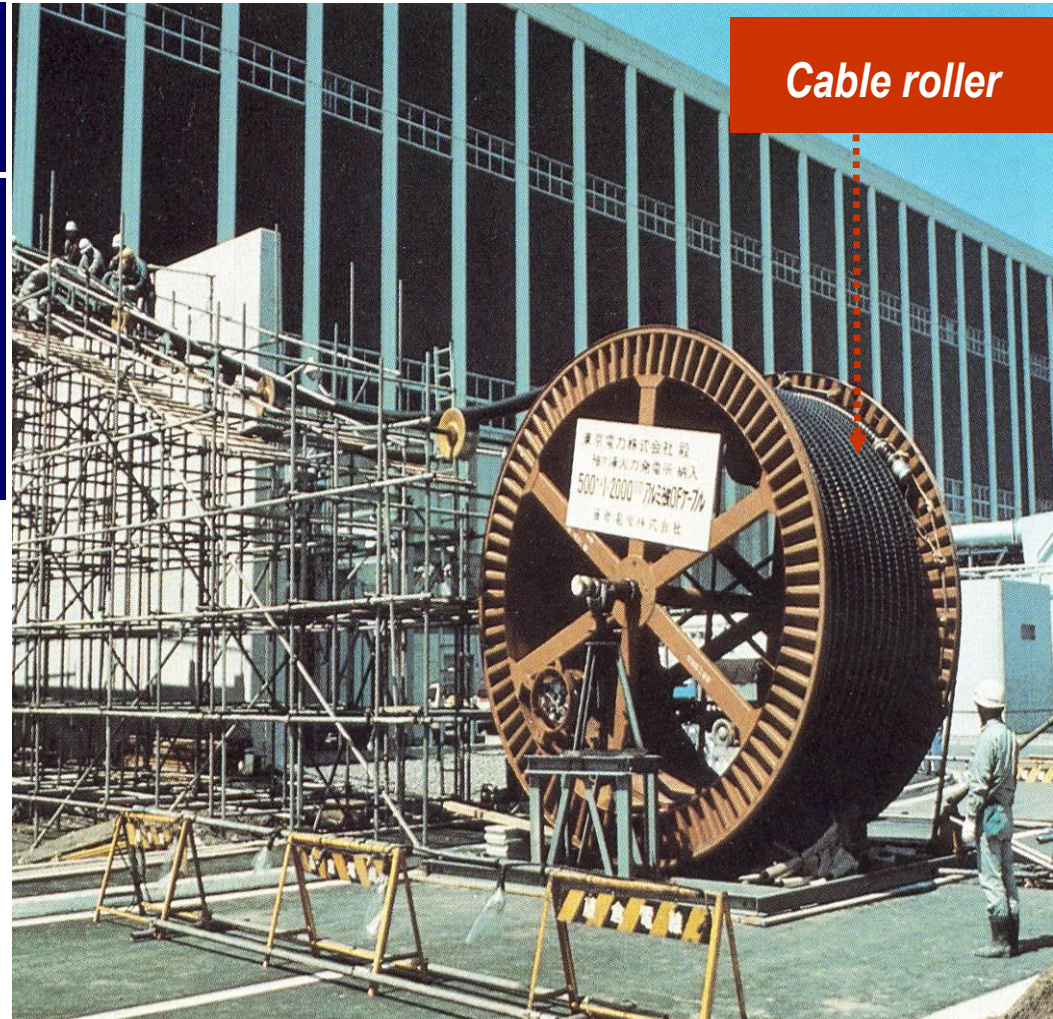
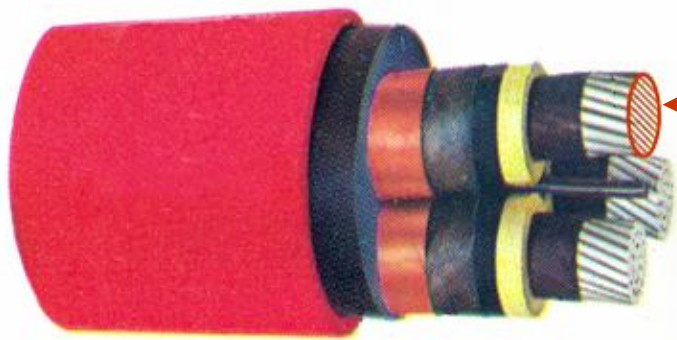
Cross section (size) of the cable (mm^2)



Application of Reactive Power Compensation

Reduction of Equipment Loading

Hence, the power rating S (kVA) of a cable is merely determined by the cross section, which must be minimized in order to reduce the investment to be made for the cable



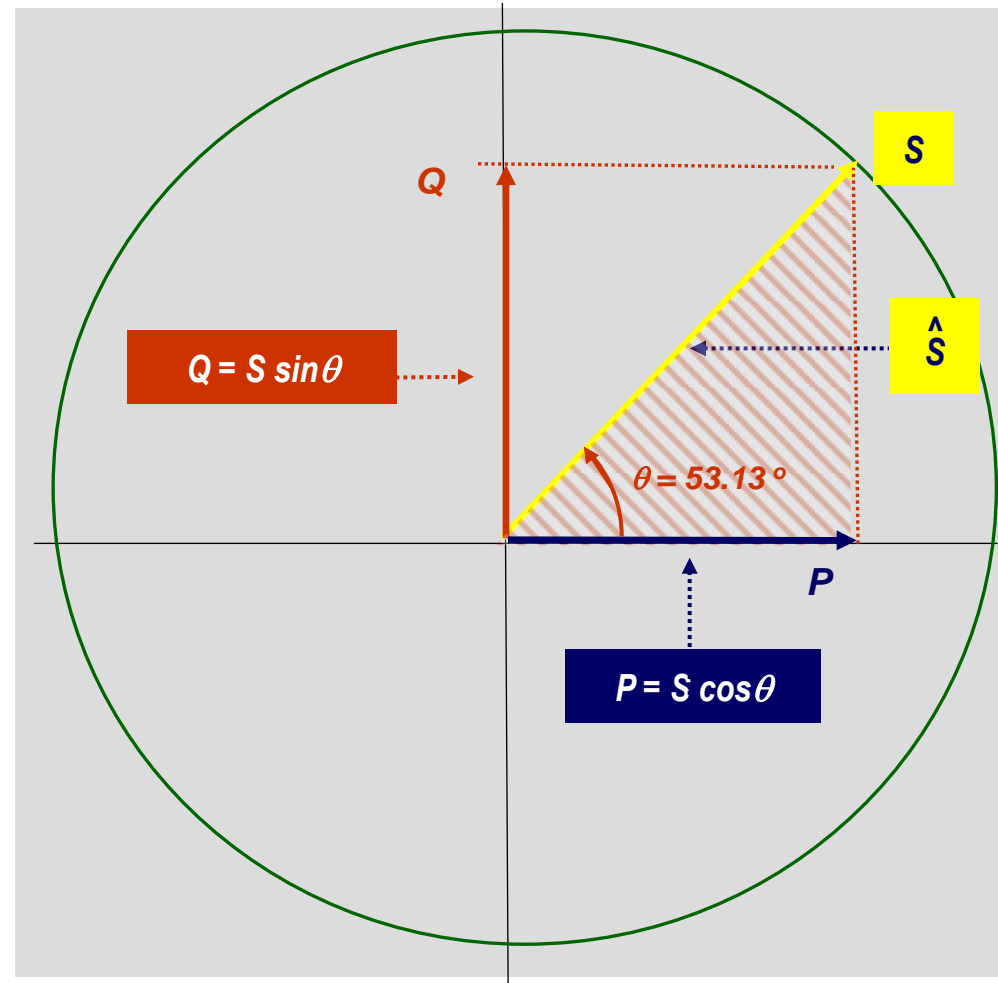
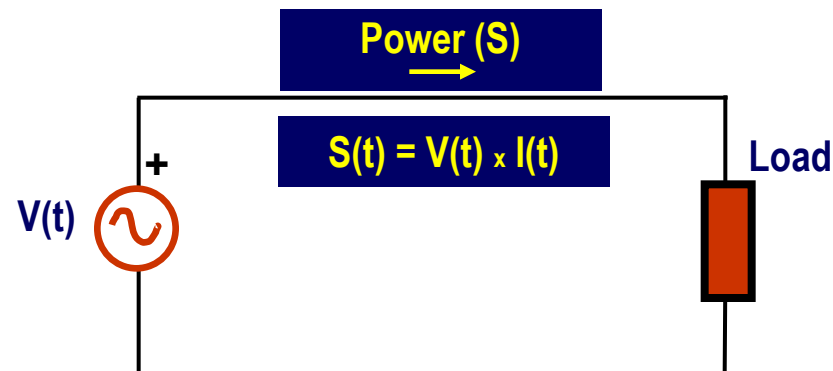
Cable roller

Application of Reactive Power Compensation

Reduction of Equipment Loading

Hence, the power rating S (kVA) of a cable is merely determined by the cross section, which must be minimized in order to reduce the investment to be made for the cable

Hence, S (kVA) must be minimized



Alternative Ways of Reducing S (kVA)

Alternative Ways of Reducing S (kVA)

a) Reducing the overall loading;

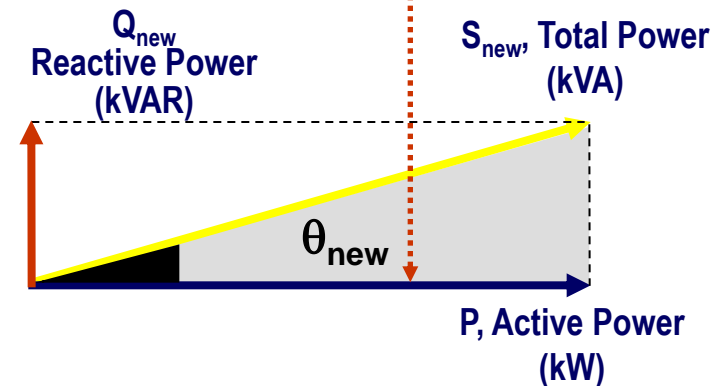
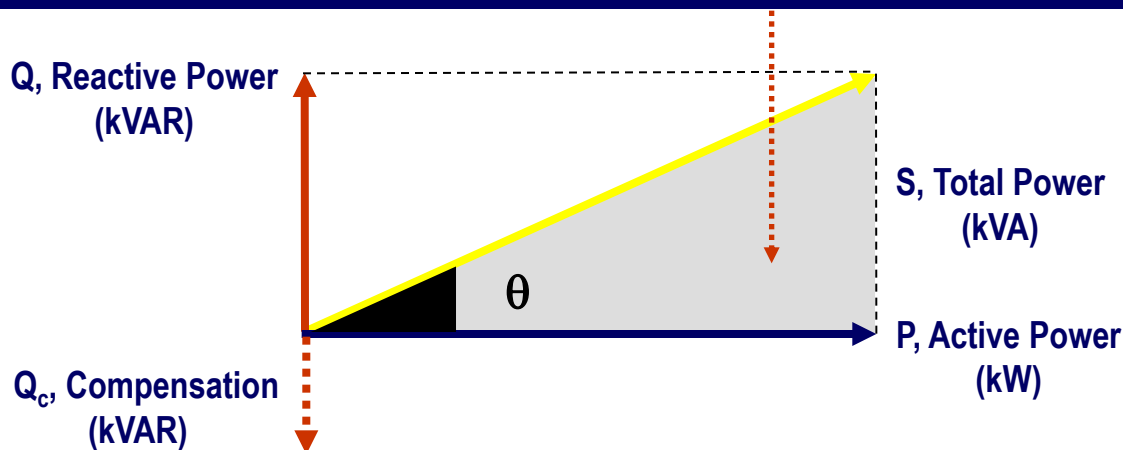
$P + jQ$ (kW + j kVAR) (Overall consumption)

Unreasonable, since the active consumption P is determined by the needs of the consumer, who consumes electricity

a) Reducing only Q (kVAR) Possible, reasonable



Please note that active power does not change after compensation



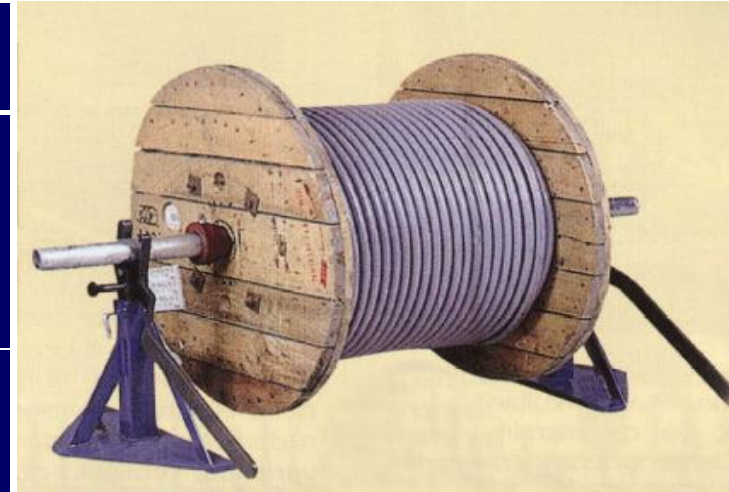
Example

Question

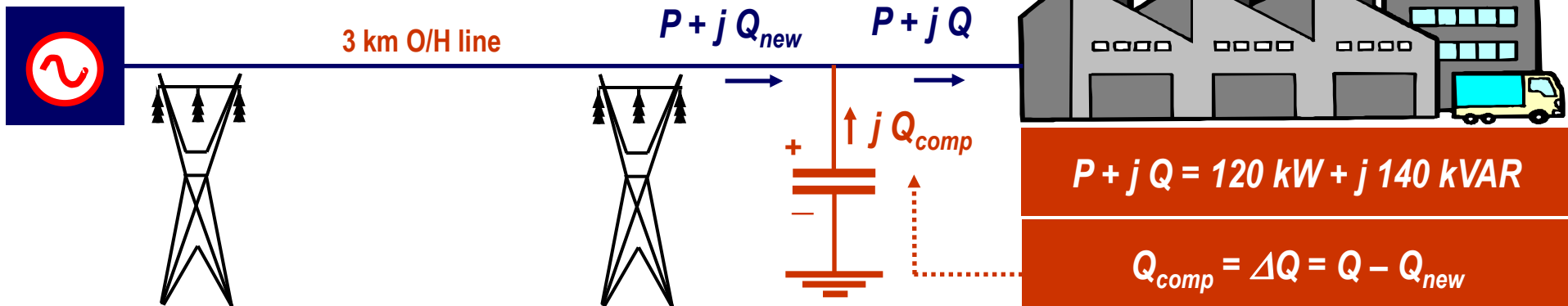
The factory shown on the RHS draws a load at 6300 V nominal voltage

$$P + jQ = 120 \text{ kW} + j 140 \text{ kVAR}$$

Calculate the amount of reactive power needed in order to raise the power factor of the factory to 0.95 (Lagging)



TEDAŞ 6300 V (rms) Mains



Example

Answer

Uncompensated (Given) Case

$$\begin{aligned} \tan \theta &= Q / P \\ &= 140 / 120 = 1.1667 \end{aligned}$$

$$\theta = \tan^{-1} 1.167 = 49.40^\circ$$

$$\text{p.f.: } \cos \theta = 0.65 \text{ (lagging)}$$

Compensated Case

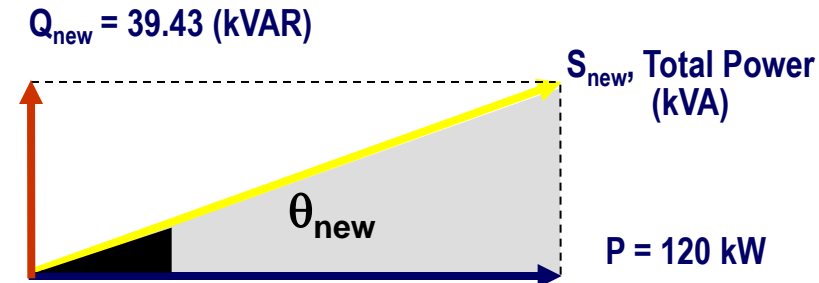
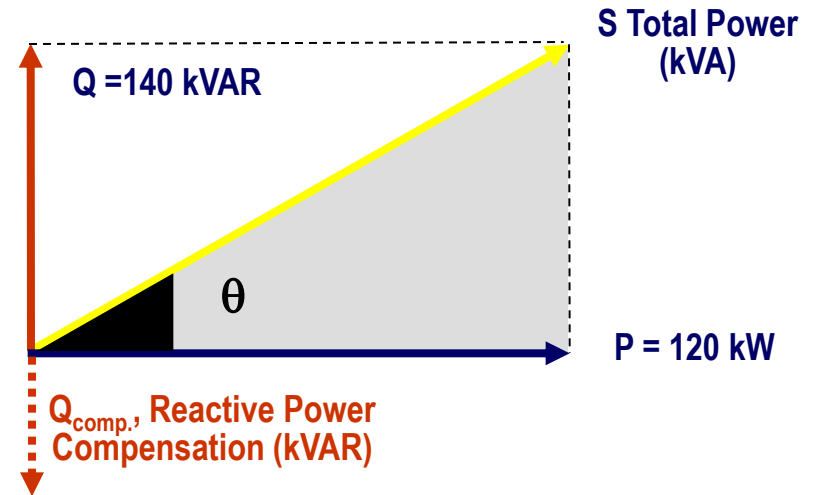
$$\cos \theta_{\text{new}} = 0.95,$$

$$\theta_{\text{new}} = \cos^{-1} 0.95 = 18.19^\circ$$

$$\tan \theta_{\text{new}} = \tan 18.19^\circ = 0.3286$$

$$\begin{aligned} \tan \theta_{\text{new}} &= Q_{\text{new}} / P \rightarrow Q_{\text{new}} = 0.3286 \times P \\ &= 39.43 \text{ kVAR} \end{aligned}$$

$$Q_{\text{comp}} = \Delta Q = Q - Q_{\text{new}} = 140 - 39.43 = 100.57 \text{ kVAR}$$

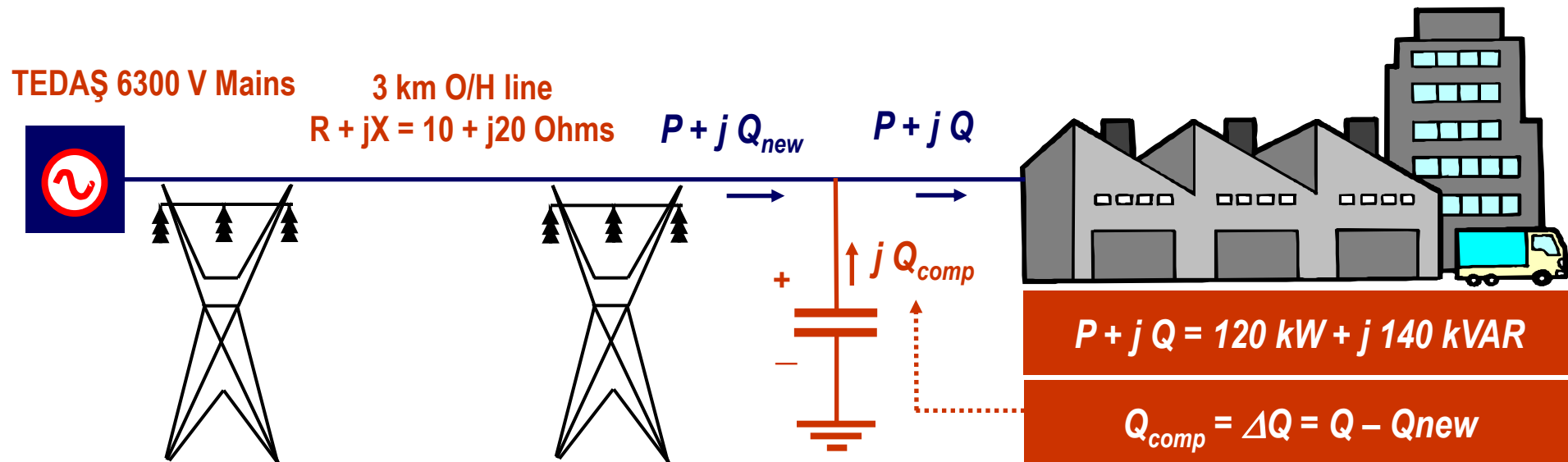


Example

Question

Now, for the previous problem, calculate the reduction in line losses as a result of this compensation by assuming that line impedance is

$$R + jX = 10 + j20 \text{ Ohms}$$



Example

$$S = VI^* \rightarrow I = S/V = \sqrt{140^2 + 120^2} / 6300$$

$$= 184.39 \times 1000 / 6300 = 29.268 \text{ Amp}$$

$$S_{\text{new}} = VI_{\text{new}}^* \rightarrow I_{\text{new}} = \sqrt{39.43^2 + 120^2} / 6300$$

$$= 126.312 \times 1000 / 6300 = 20.049 \text{ Amp}$$

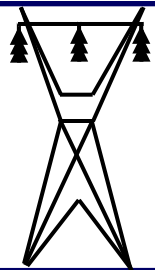
$$P_{\text{loss}} = RI^2 = 10 \times 29.268^2 = 8566.39 \text{ Watts}$$

$$P_{\text{loss-new}} = RI_{\text{new}}^2 = 10 \times 20.049^2 = 4019.84 \text{ Watts}$$

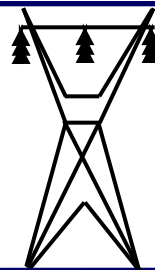
$$\Delta P_{\text{loss}} = 8566.39 - 4019.84$$

$$= 4546.55 \text{ Watts}$$

TEDAŞ 6300 V Mains



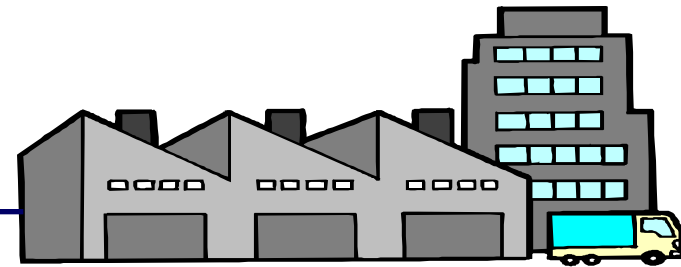
3 km O/H line
 $R + jX = 10 + j20 \text{ Ohms}$



$P + jQ_{\text{new}}$



$P + jQ$



$P + jQ = 120 \text{ kW} + j140 \text{ kVAR}$

$$Q_{\text{comp}} = \Delta Q = Q - Q_{\text{new}}$$

Example

Now, calculate the return rate of the investment to be made for the compensator, by assuming that the retail price of electricity is 16 Cents/kWh and price of capacitor is 184.41 USD/kVAR

$$\Delta P_{loss} = 8566.39 - 4019.84 = 4546.55 \text{ Watts}$$

$$\text{Investment} = 100.57 \text{ kVAR} * 184.41 \text{ USD/kVAR} \\ = 18546,11 \text{ USD}$$

$$\text{Saving} = 4546.55 / 1000 * 16 \text{ Cent/kWh} / 100 \\ = 0.7274 \text{ USD / hour}$$

$$\text{Return Rate} = \text{Investment} / \text{Saving} \\ = 10057.00 / 0.7274 \\ = 13825.9 \text{ hours} = 576.8 \text{ days} = 1.58 \text{ years}$$

CORPORATE

PRODUCTS

SERVICES

TECHNICAL RESOURCES

LV-ACB™ List Price

Low Voltage Automatic Capacitor Banks

480 VOLT AUTOMATIC CAPACITOR BANKS

| BANK RATING (KVAR) | STEP X KVAR | MODEL NUMBER | LIST PRICE |
|--------------------|-------------|------------------|------------|
| 150 | 3 X 50 | 150LVA480F2B | \$7,526 |
| 200 | 4 X 50 | 200LVA480F2B | \$8,389 |
| 250 | 5 X 50 | 250LVA480F2B | \$8,864 |
| 300 | 6 X 50 | 300LVA480F2B | \$9,727 |
| 350 | 7 X 50 | 350LVA480F2B | \$10,202 |
| 400 | 4 X100 | 400LVA480F2B100 | \$10,580 |
| 400 | 8 X 50 | 400LVA480F2B | \$11,065 |
| 450 | 9 X 50 | 450LVA480F2B | \$11,540 |
| 500 | 5 X 100 | 500LVA480F2B100 | \$11,918 |
| 500 | 10 X 50 | 500LVA480F2B | \$12,404 |
| 550 | 11 X 50 | 550LVA480F2B | \$12,830 |
| 600 | 6 X 100 | 600LVA480F2B100 | \$13,256 |
| 600 | 12 X 50 | 600LVA480F2B | \$13,742 |
| 650 | 13 X 50 | 650LVA480F2B | \$12,280 |
| 700 | 7 X 100 | 700LVA480F2B100 | \$14,594 |
| 700 | 14 X 50 | 700LVA480F2B | \$15,080 |
| 750 | 15 X 50 | 750LVA480F2B | \$15,506 |
| 800 | 8 X 100 | 800LVA480F2B100 | \$15,933 |
| 800 | 16 X 50 | 800LVA480F2B | \$16,418 |
| 900 | 9 X 100 | 900LVA480F2B100 | \$17,174 |
| 1000 | 10 X 100 | 1000LVA480F2B100 | \$18,414 |

Example

Question

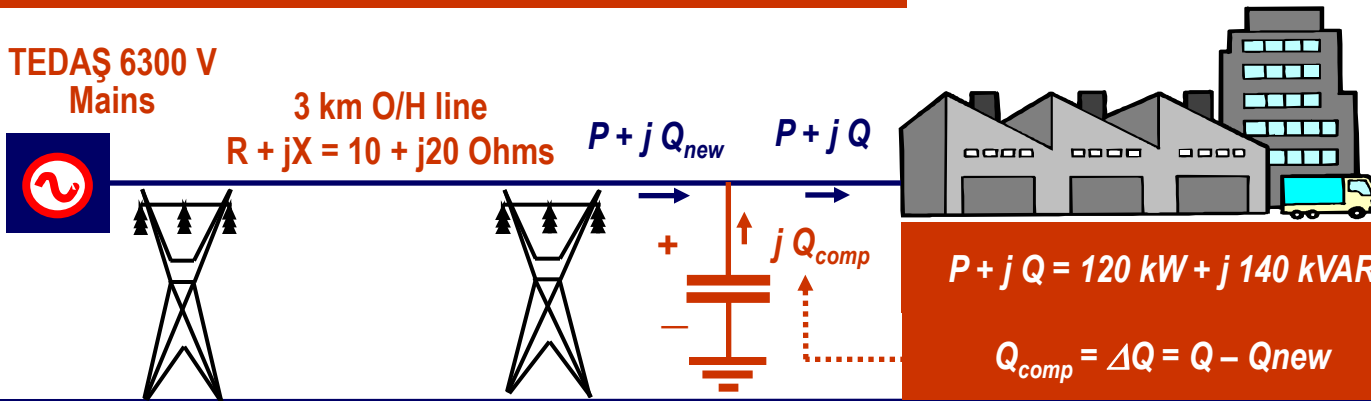
Now, for the previous problem, determine the minimum cross section of the line for the alternative cases, when line is compensated and uncompensated

$$I_{new} = 20.495 \text{ Amp}$$

$$I_{initial} = 29.268 \text{ Amp}$$

The cheaper alternative

| Cross Section (mm ²) | Current Capacity (Amp) |
|--------------------------------------|-----------------------------|
| 1.0 | 12,0 |
| 1.5 | 16,0 |
| 2.5 | 21,0 |
| 4.0 | 27,0 |
| 6.0 | 35,0 |
| 10.0 | 48,0 |
| 16.0 | 65,0 |
| 25.0 | 88,0 |
| 35.0 | 110,0 |
| 50.0 | 140,0 |
| 70.0 | 175,0 |
| 95.0 | 215,0 |
| 120.0 | 225,0 |



Question

Question

Now, for the previous problem, calculate the shunt capacitance in Farads needed for the amount of compensation found above

$$Q_{comp} = \Delta Q = Q - Q_{new} = 140 - 39.43 = 100.57 \text{ kVAR}$$

$$Q_{comp} = V I_{comp}^* \rightarrow I_{comp} = Q_{comp} / V = 100570 \text{ VA} / 6300 \text{ V} = 15.963 \text{ Amp}$$

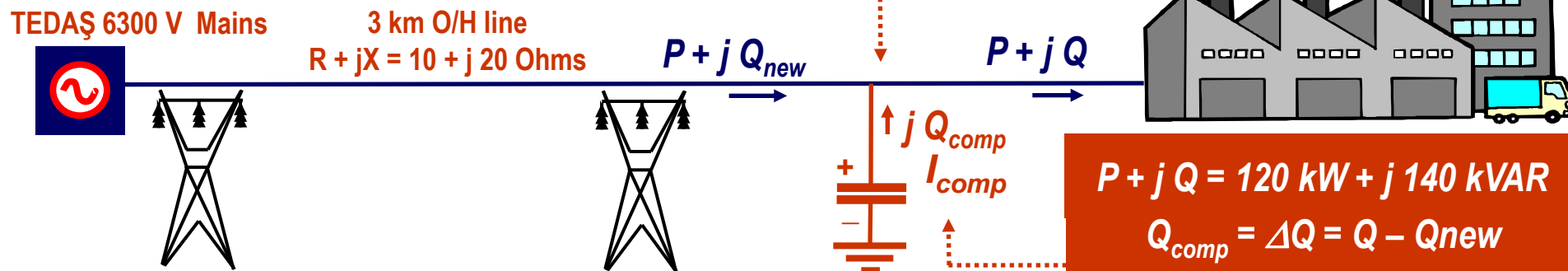
$$X_{comp} = V / I_{comp} = 6300 / 15.963 = 394.65 \text{ Ohms}$$

$$X_{comp} = 1 / (j\omega C)$$

$$C = 1 / (j\omega X) = 1 / (314.15 \times 394.65) = 123.98 \text{ mF}$$

$$Q_{new} = Q + Q_{comp}$$

$$Q_{comp} < 0$$

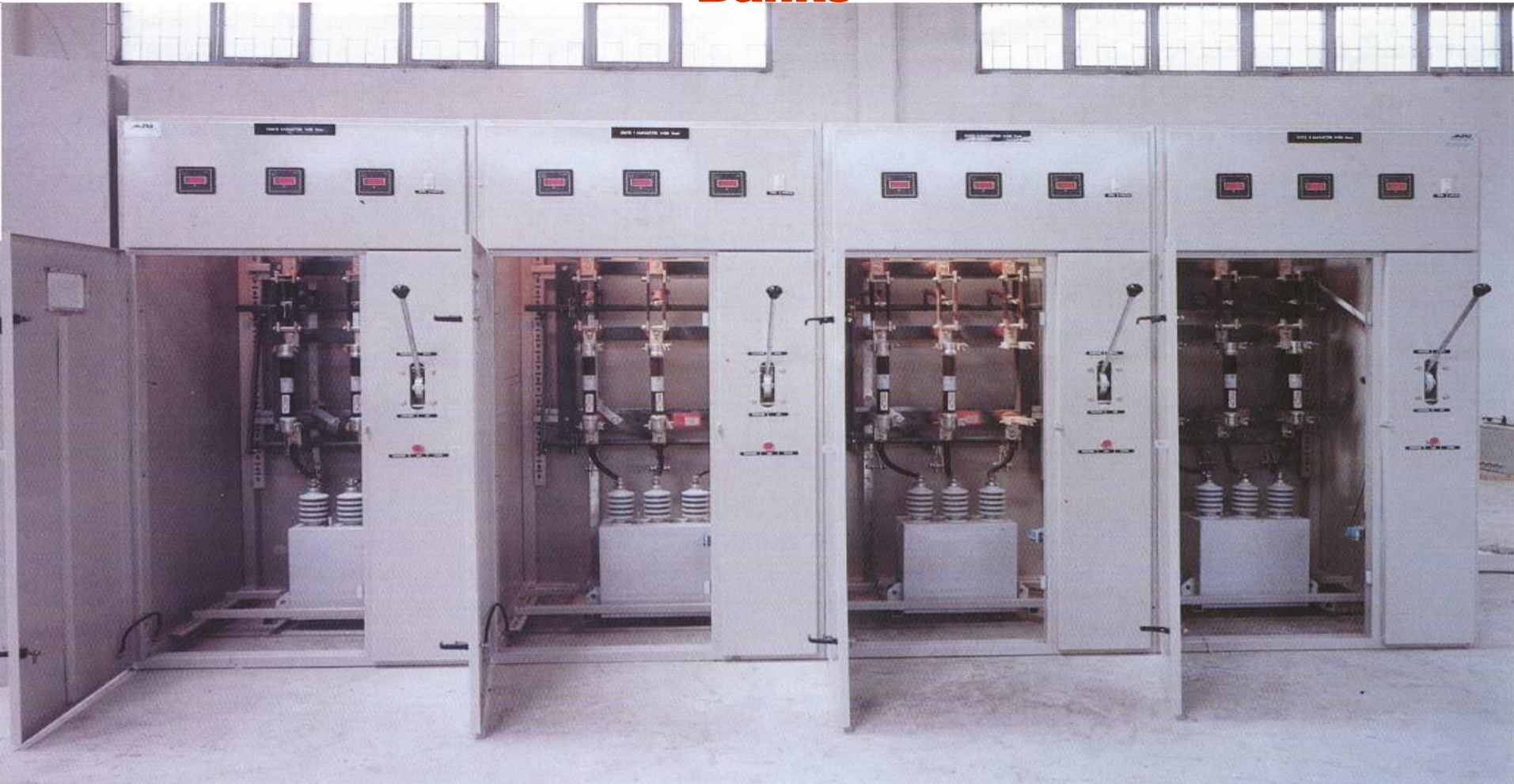


Medium Voltage Capacitor Banks

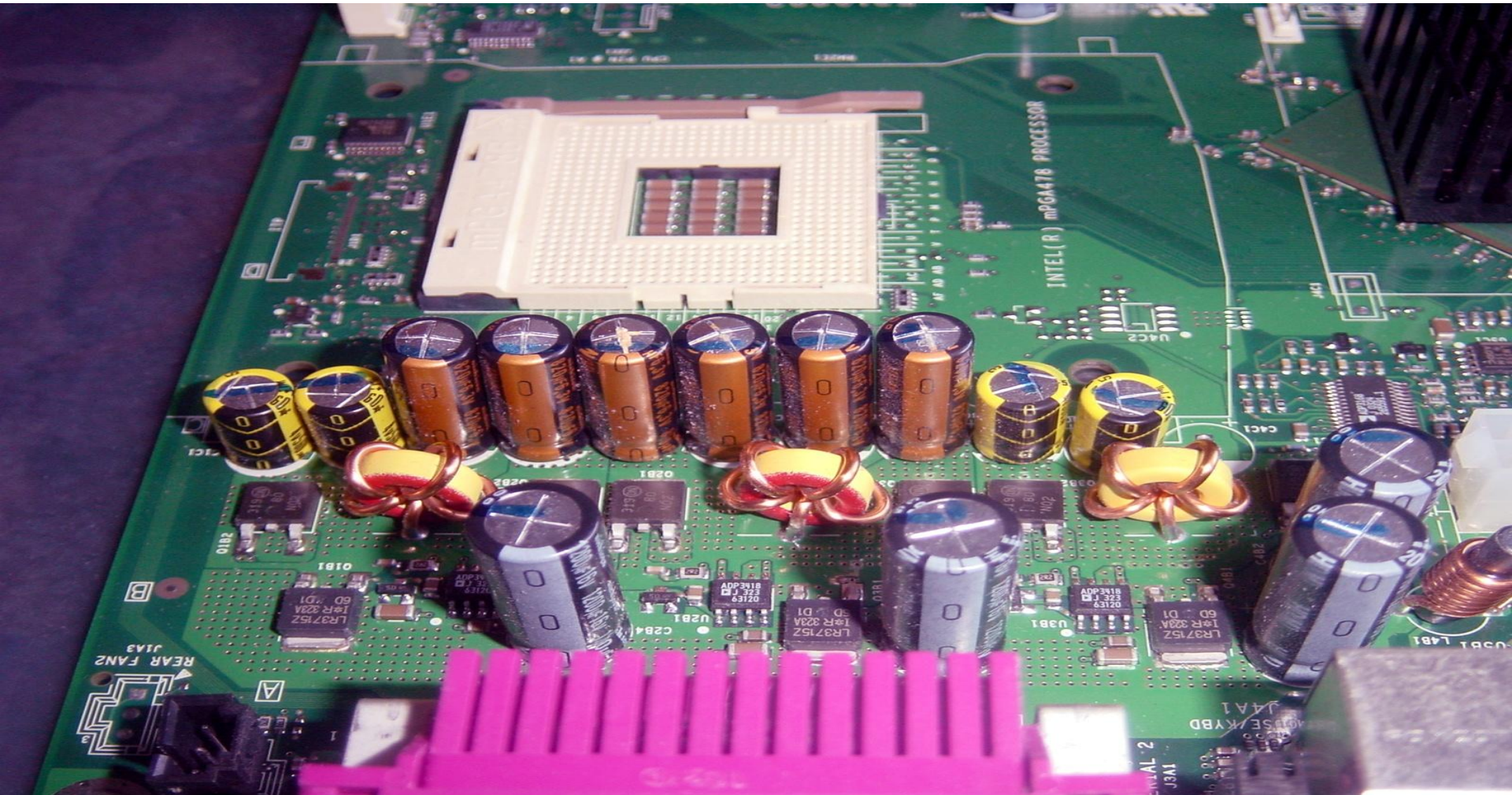
Shunt connection of large capacity capacitors in power systems



Installation of MV Capacitor Banks



Electronic Capacitors in a Motherboard



Another Example

- Early in the history of electricity, Thomas Edison's General Electric company was distributing DC electricity at 110 volts in the United States.
- Then Nikola Tesla devised a system of three-phase AC electricity at 240 volts. Three-phase meant that three alternating currents slightly out of phase were combined in order to even out the great variations in voltage occurring in AC electricity. He had calculated that 60 cycles per second or 60Hz was the most effective frequency. Tesla later compromised to reduce the voltage to 110 volts for safety reasons.

Another Example

- Europe goes to 50 Hz:
- With the backing of the Westinghouse Company, Tesla's AC system became the standard in the United States. Meanwhile, the German company AEG started generating electricity and became a virtual monopoly in Europe. They decided to use 50 Hz instead of 60 Hz to better fit their metric standards, but they kept the voltage at 110 V.
- Unfortunately,
- 50 Hz AC has greater losses and is not as efficient as 60 HZ.

Another Example

- Due to the slower speed, 50Hz electrical generators are 20 % less effective than 60Hz generators. Electrical transmission at 50 Hz is about 10-15 % less efficient. 50Hz transformers require larger windings and 50 Hz electric motors are less efficient than those meant to run at 60Hz. They are more costly to make to handle the electrical losses and the extra heat generated at the lower frequency.
- Europe goes to 220 V
- Europe stayed at 110 V AC until the 1950s, just after World War II. They then switched over to 220 V for better efficiency in electrical transmission. Great Britain not only switched to 220 V, but they also changed from 60Hz to 50 Hz to follow the European lead. Since many people did not yet have electrical appliances in Europe after the war, the change-over was not that expensive for them.
- U.S. stays at 110 V, 60Hz

Another Example

- The United States also considered converting to 220 V for home use but felt it would be too costly, due to all the 110 V electrical appliances people had. A compromise was made in the U.S. in that 220 V would come into the house where it would be split to 110 V to power most appliances. Certain household appliances such as the electric stove and electric clothes dryer would be powered at 220 V.

Did everybody follow this part carefully ?

